



Energy Analysis Techniques

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What is energy conservation?



Three simple ways to save energy

1. By not doing things – e.g. not traveling
2. By doing things at reduced quality – traveling in a two wheeler or may be cycle
3. By doing things as before or better with lower energy use – e.g. using more efficient cars, or combining many trips into one or car pooling

Energy conservation

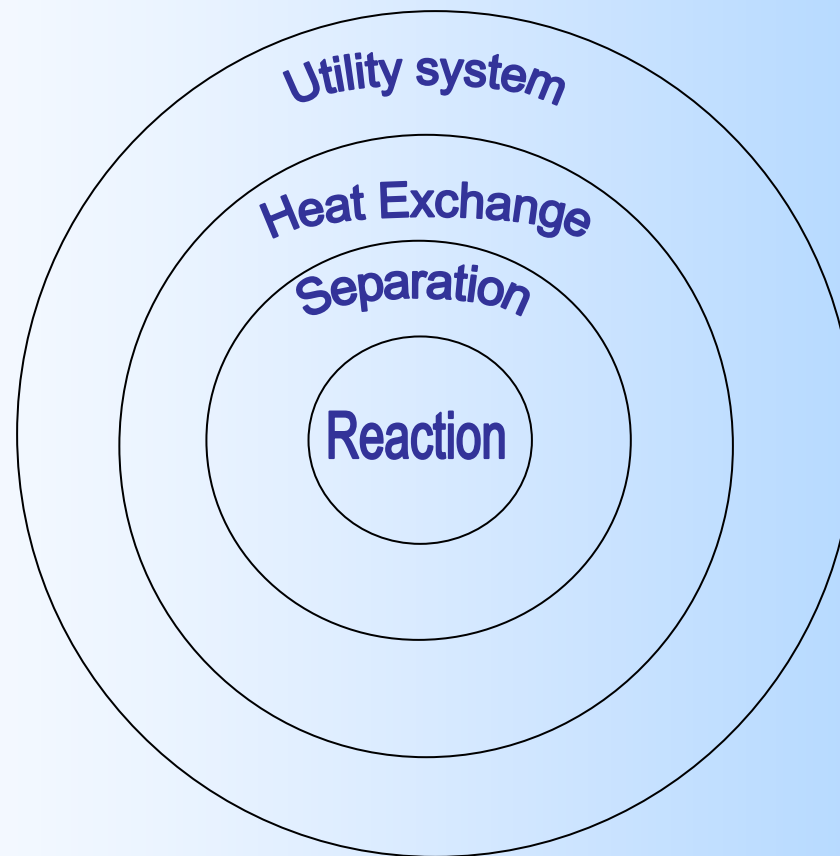


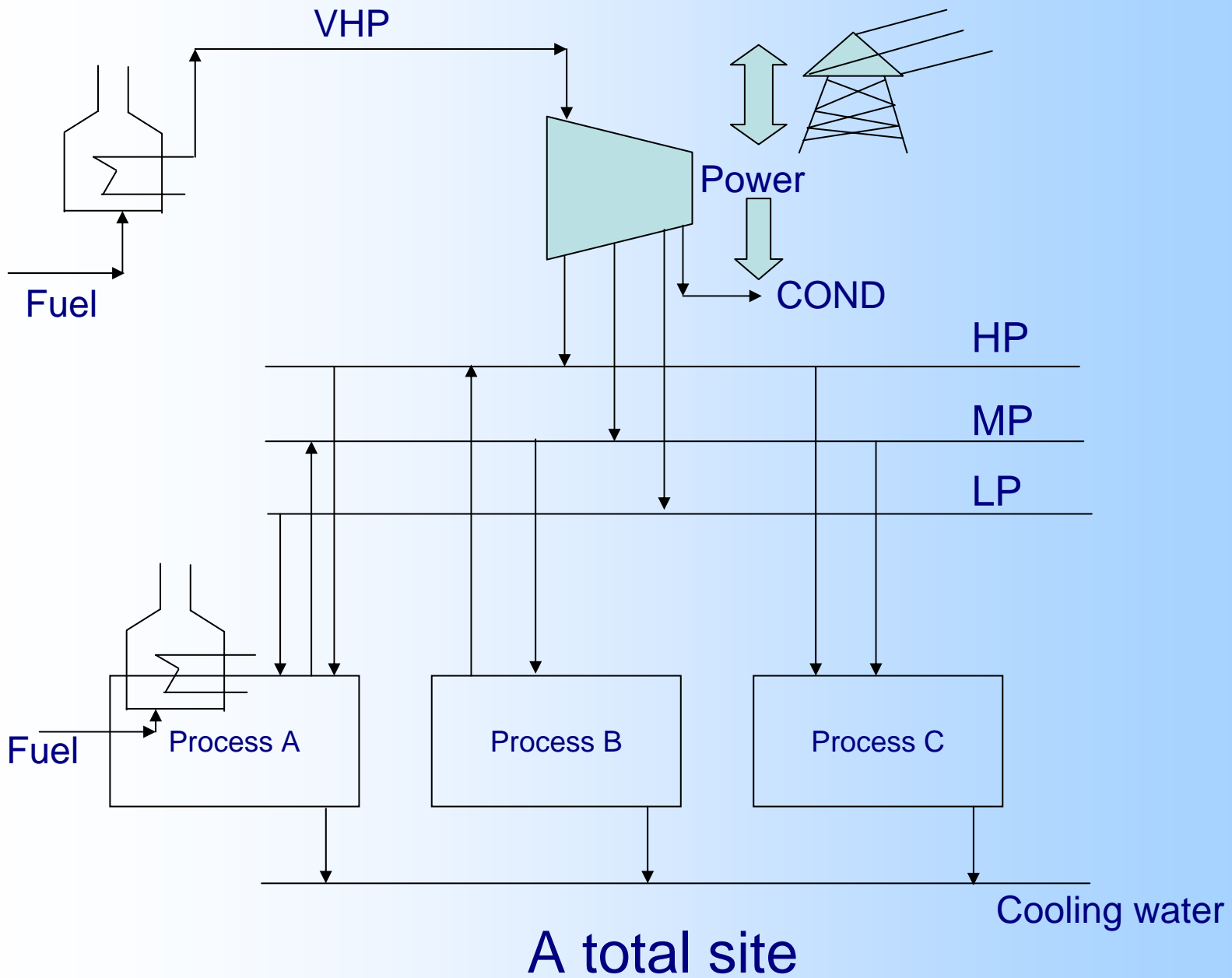
- Realizing the objectives of the operation / action with lower energy or resource consumption without compromising the quality of outcome.

Need for energy conservation



- Limited resources
- Cost competitiveness
- Rising Energy costs
- Global environmental concerns
- Regulatory requirements to reduce emissions





Complex interactions



- Process to Process
 - Intra and inter process both
- Process to utility
- Utility to utility
- Process to process through utility

Approach to energy analysis



- Conventional approach
 - Individual equipment performance
 - Standalone analysis
 - Global impact not considered
- Integrated approach
 - Systems approach accounting for all site interactions
 - Identify potential areas
 - Establish benefits
 - Translate them to global level
 - Target global optimization of energy and resource consumption

Integrated energy analysis - Methodology



- Individual equipment performance analysis
- Process audit
- Utility system analysis
- Integrated system analysis
- Monitoring and targeting

Equipment performance analysis



- Fired heaters
 - Heater efficiency estimation
- Boilers
 - Boiler efficiency estimation
- Compressors
 - Establish polytropic and overall efficiency
- Pumps
 - Establish pump performance & VSD application
- Fin fan coolers
 - Coolers performance & VSD application

Boilers / Fired heaters



- Efficiency estimation by direct and indirect methods
- Indirect method gives better insight towards the losses and helps identifying the potential area
- Efficiency improvement
- Soot deposit, peep holes, dampers

Furnace efficiency



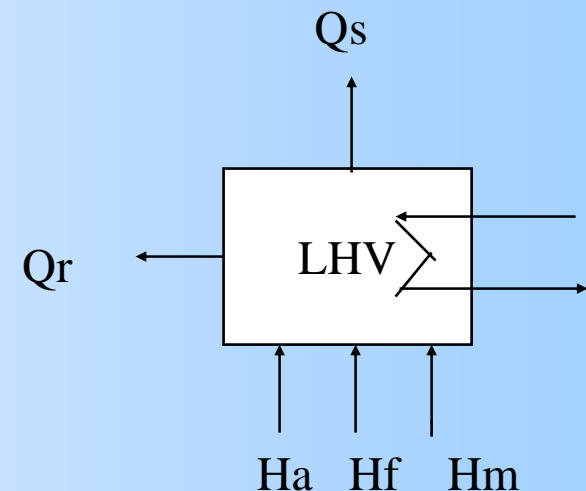
• THERMAL EFFICIENCY OF HEATER

- LHV : LOWER HEATING VALUE OF THE FUEL
- HM : ENTHALPY OF ATOMISING MEDIA
- HA : ENTHALPY OF AIR ABOVE 15.5°C
- HF : ENTHALPY OF FUEL
- QS : HEAT CONTENT OF STACK GASES
- QR : HEAT LOSS FROM HEATER SURFACE

$$\eta = \frac{\text{Total Heat Absorbed}}{\text{Total Heat Input}} \times 100$$

$$= \frac{\text{Total Heat Input} - \text{Total Heat Losses}}{\text{Total Heat Input}} \times 100$$

$$= \frac{LHV + H_a + H_f + H_m - (Q_r + Q_s)}{LHV + H_a + H_f + H_m} \times 100$$



Compressor efficiency



- Establish polytropic efficiency
- Establish overall efficiency
- Real work transferred to fluid
- Fine tune feed suction conditions / inter-cooling / bearing losses / recycle flow



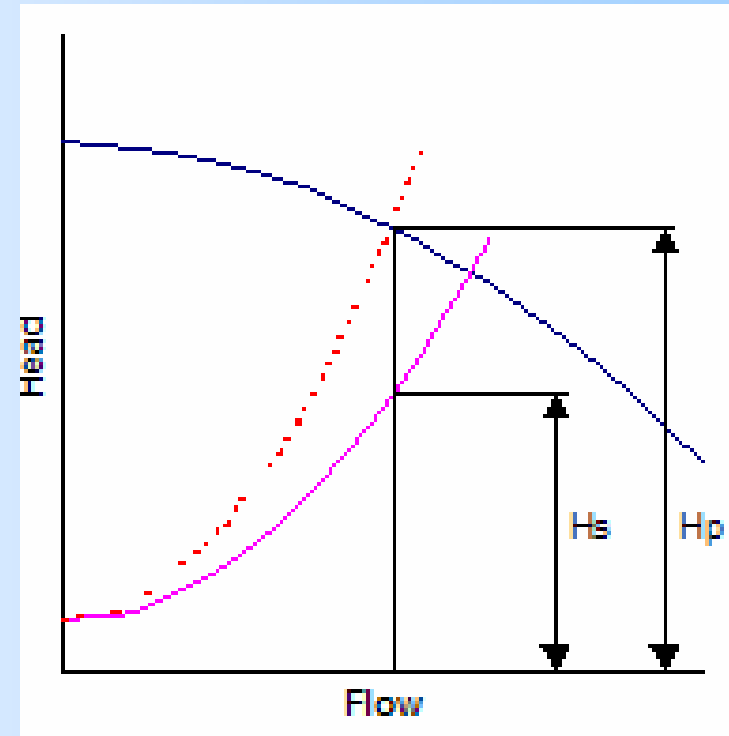
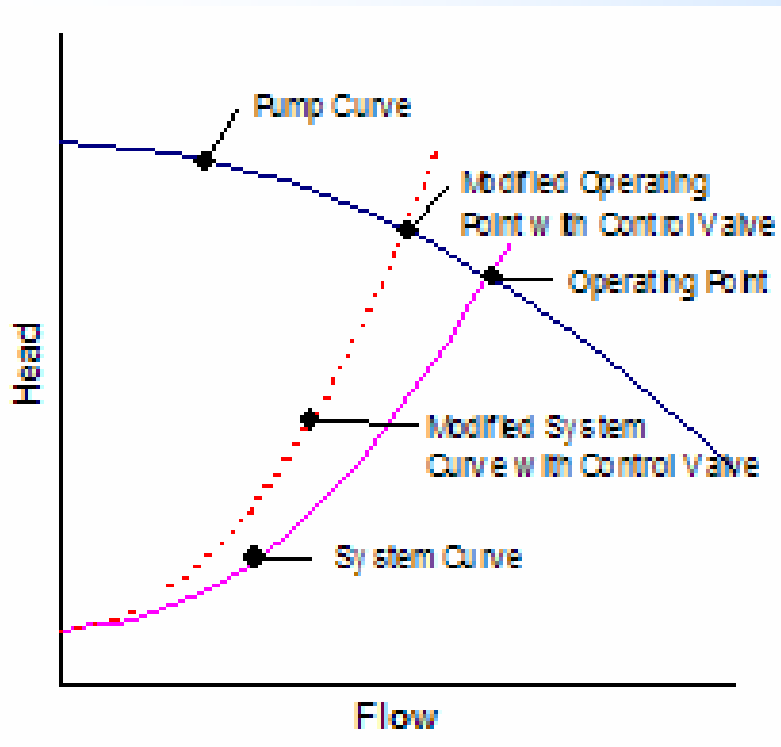
OPERATING DATA			
Stage - I			
	Suction	Discharge	
Pressure, psia	235.6	437	
Temperature, °F	96.9	231.8	
Compressibility	1.0003	1.0076	
Flow lb/min	556.54		
Cp/Cv	1.30	1.28	
Cp/Cv (Avg)	1.29		
Stage 1			
Gas composition	Mole (f) we	Mol.Wt	Mol.m, w
C1	0.089	16.043	1.427827
C2	0.054	30.07	1.62378
C3	0.04	44.097	1.76388
I-C4	0.013	58.123	0.755599
N-C4	0.015	58.123	0.871845
I-C5	0.01	72.15	0.7215
C6+	0.009	86.117	0.775053
C2H4		28	0
C3H6		42	0
C3H4		40	0
C4H8		56	0
C4H4		52	0
H2	0.75	2.016	1.512
CO		28.01	0
Air		28.963	0
CO2	0.015	44.01	0.66015
N2	0.005	28.013	0.140065
H2S		34.08	0
O2		31.999	0
H2O		18.015	0
Total	1		10.25

K-201		
Gas Flow	Stage - I	
Mol. Wt	10.25	
Wt flow Lb/min	556.54	
Operating parameters		
	Stage - I	
	Suction	Discharge
Temp., °R	556.90	691.80
	Stage - I	
Polytropic n	1.541	
cp/cv (Avg)	1.291	
Av. Comp. Factor	1.004	
Head Polytropic, Ft	58133	
BHPp gas	980	
KW Gas	731	
Head J/kg	173784	
Total Gas Power KW	731	
Overall Efficiency %	55.6	
Polytropic Efficiency	64.3	
Motor Drive		
Amps	372.4	
Volts	2400	
Power Factor	0.85	
Motor KW	1316	

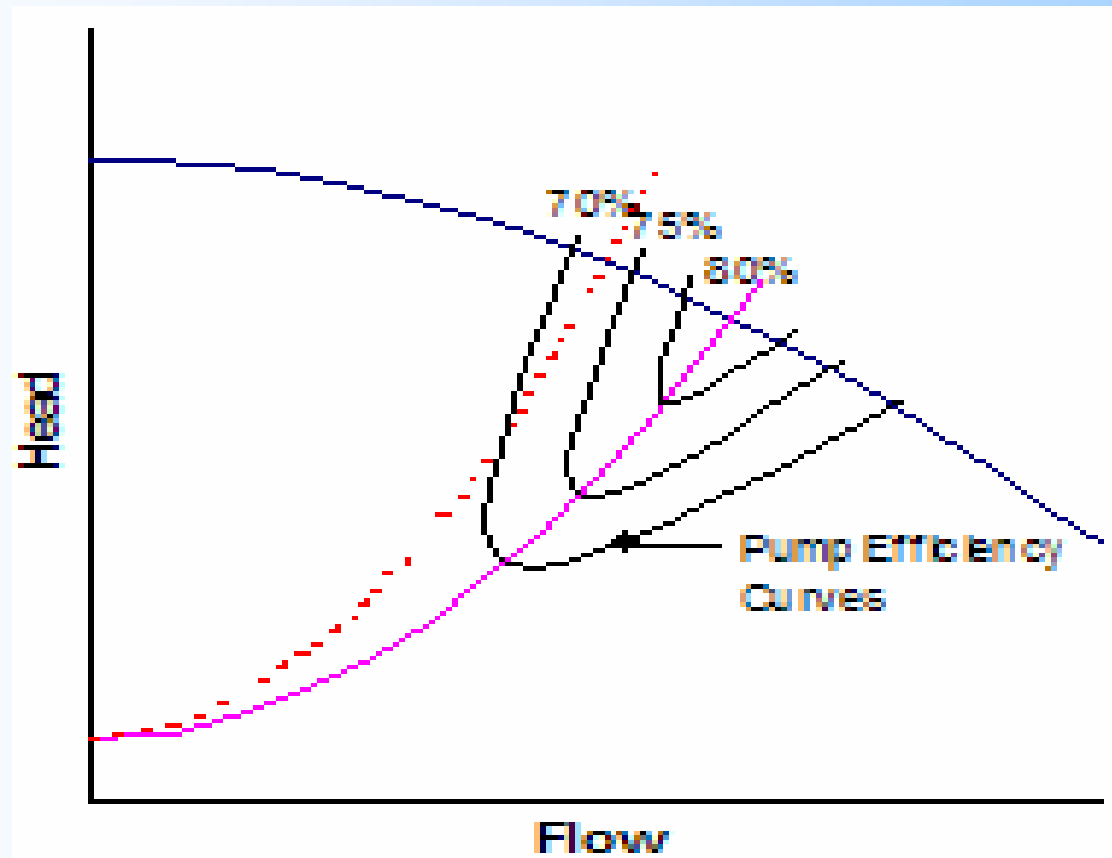


- Establish current performance
- Compare it with design operating point on characteristic curves
- Optimize power consumption by choosing appropriate impeller or through application of VSD

Throttling losses

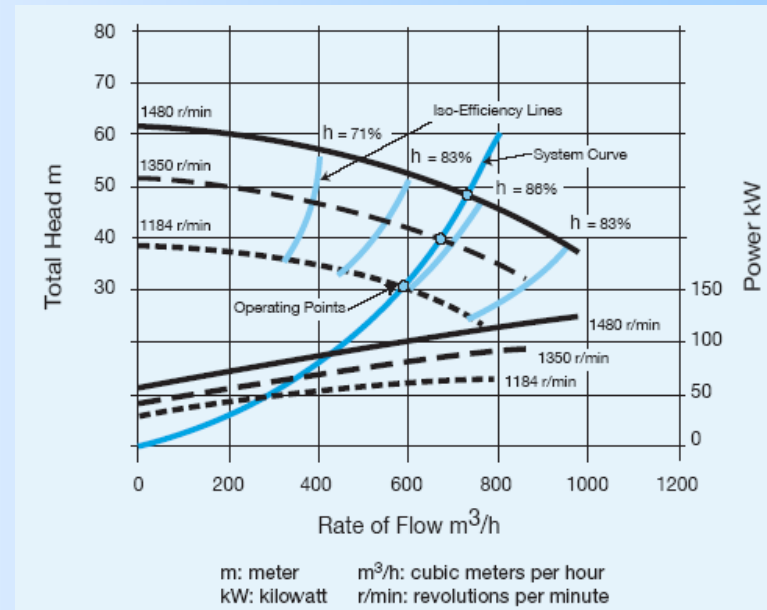
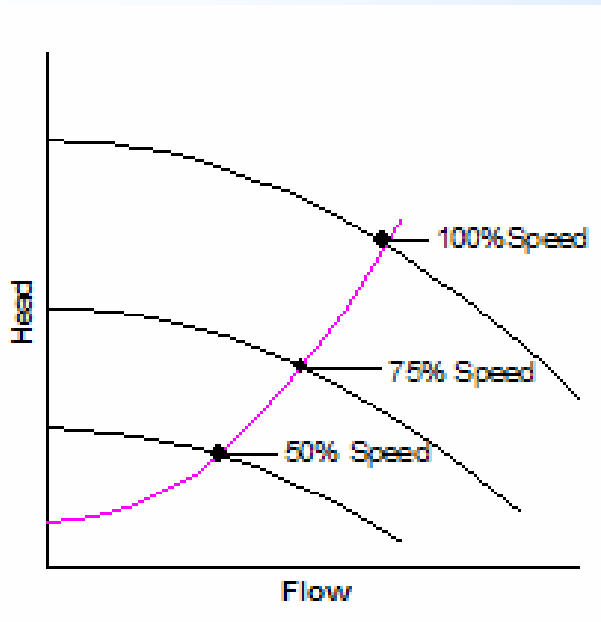


Throttling losses



VSD Application in pumps

- When speed control is employed to control the pump flow the pump curve moves up and down the system curve.
- This ensures just enough energy is supplied to get the desired flow



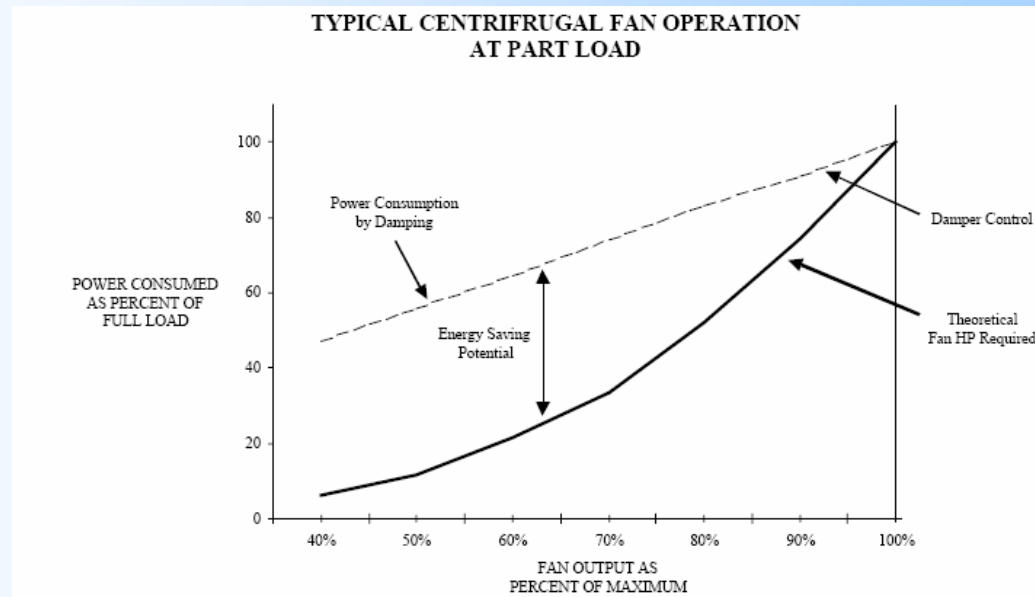
Applications of VSD on fans



- Normally the procedure applied for pumps can be extended for a VSD application on a fan also and the same affinity laws are applicable.
- These correspond to variation in flow requirement by the system.
- For cases where the variation in flow is due to meeting the process requirement at varying utility property due to ambient limitation, process analysis or equipment evaluation might be required

Application of VSD on fans

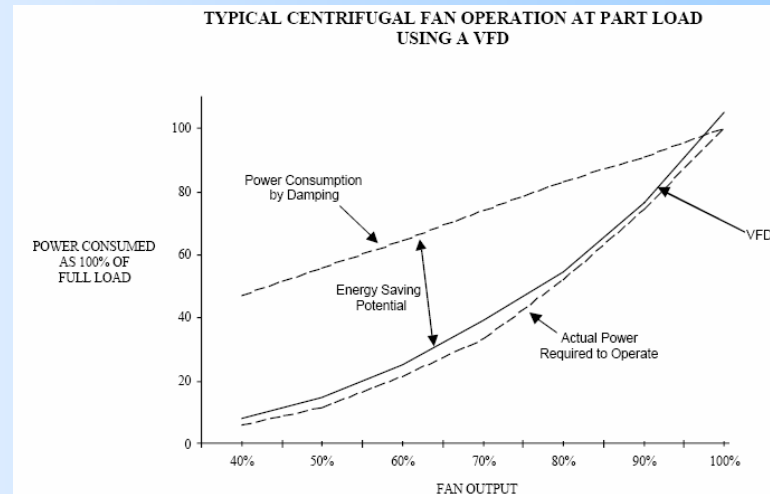
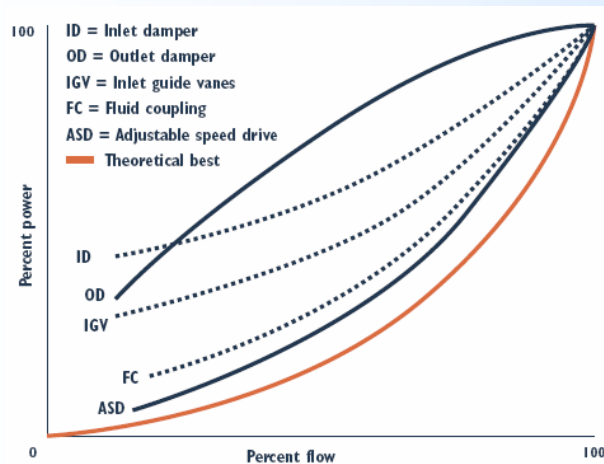
- Flow control through restricting control device such as throttling, damping and recirculating of flow has a direct bearing on the fan/blower energy consumption.
- The energy saving through VSD results from eliminating the damping and moving closer to the theoretical minimum requirement.



VSD POWER SAVING



- The effect of various types of control mechanism on power utilization of fans is depicted below



Fin fan cooler



- These are product or process stream cooling exchangers using air as the cooling medium.
- For geographical locations where there is a wide variation of temperature throughout the year and day and night.
 - The flow of air through these exchangers have to be varied to meet the process requirement.
 - In actual for system with multi fans shutting of fans is practiced
 - Other method available is fans with multi pitch control which is adjusted at extreme conditions.

Fin fan coolers



- Rate the current operation
- Study variation in ambient conditions
- Power savings through application of VSD

VSD on fan fin (015-e-263)



Fin Fan Cooler Evaluation		DESIGN SIMULATION	
Geometry (Tubes with radial fins)			
No of fans	2		
Air flow	189.5 kg/s		
Air inlet T	41.1 °C		
Air Exit T	68.7 °C		
Cp	0.239 kcal/kg.°C		
Duty	4.50 MMKcal/h	4.50	
Process f	29.67 kg/s		
Proc Inlet T	146.1 oC		
Proc Out T	65.6 oC		
U process	528.0 kcal/h.m ² .C	528	
Design U bare	kcal/h.m ² .C		
Types of fins			
No of fins/ m	394		
Fi OD	mm	57.15	
Fin Ht	mm	15.88	
Fin thk	mm	0.4064	
Fin spacing	mm	2.54	Summer High Temperature
Tube OD	mm	25.4	
Tube ID	mm	21.8	
Tube L	m	12.2	
Effective L	m	12.2	
Tube pitch	mm	63.5	
Total Finned tubes	306		
Rows	5		
Fin Thc W/m.K	208		
Fan dia	m	3.962	
Air side calculation			
Geometric factors			
Unfinned surface	0.080 m ² /m		6161
Finned surface	1.652 m ² /m	ft2	m2
Bare external surface	0.080 m ² /m	3206	298
FAR	0.456 Table - 9.2		56
Effective Fin ht	0.021 m (Tab-9.3)		57
			226
Cooler face area	47.91 m ²		
Flow area between Tubes	21.83 m ²	2 bundle	3937 mm
Fan Opening area	24.67 m ²	Effective	3930 mm
		Overall	mm
			end elevation
Air velocity			
Flow rate standard m ³ /s	154.15	T	15.5 P
Flow rate at fans m ³ /s	167.87	T	41.1 P
Standard Vel Bet Tu	7.06 m/s		
Velocity Thru fan openings	3.50 m/s		
Fin Efficiency and coefficient			
Htc to the fins alpha'	56.78 W/m ² .K		
(me)x(lfe)	0.757		
Fin Efficiency Omega	0.845		
Effective fin side Htc	1048.9 W/m ² .K	903.4 kcal/h.m ² .K	185 Btu/hr.ft ² .°F
Pressure loss and power consumption			
Bundle loss	15.3 mmWC		
Fan & Plenum loss	0.8 mmWC	Rho based on summer high temp	
Total loss	16.1 mmWC		
Required Fan Power	26.5 KW	35.5 HP	

Fin Fan Cooler Evaluation		CASE-1	
Geometry (Tubes with radial fins)			
No of fans	2		
Air flow	146.2 kg/s		
Air inlet T	35.8 °C		
Air Exit T	71.6 °C		
Cp	0.239 kcal/kg.°C		
Duty	4.50 MMKcal/h	4.50	
Process f	29.67 kg/s		
Proc Inlet T	146.1 oC		
Proc Out T	65.6 oC		
U process	528.0 kcal/h.m ² .C	528	
Design U bare	kcal/h.m ² .C		
Types of fins			
No of fins/ m	394		
Fi OD	mm	57.15	
Fin Ht	mm	15.88	
Fin thk	mm	0.4064	
Fin spacing	mm	2.54	Summer High Temperature
Tube OD	mm	25.4	
Tube ID	mm	21.8	
Tube L	m	12.2	
Effective L	m	12.2	
Tube pitch	mm	63.5	
Total Finned tubes	306		
Rows	5		
Fin Thc W/m.K	208		
Fan dia	m	3.962	
Air side calculation			
Geometric factors			
Unfinned surface	0.080 m ² /m		6161
Finned surface	1.652 m ² /m	ft2	m2
Bare external surface	0.080 m ² /m	3206	298
FAR	0.456 Table - 9.2		56
Effective Fin ht	0.021 m (Tab-9.3)		57
			226
Cooler face area	47.91 m ²		
Flow area between Tubes	21.83 m ²	2 bundle	3937 mm
Fan Opening area	24.67 m ²	Effective	3930 mm
		Overall	mm
			end elevation
Air velocity			
Flow rate standard m ³ /s	118.94	T	15.5 P
Flow rate at fans m ³ /s	127.34	T	35.8 P
Standard Vel Bet Tu	5.45 m/s		
Velocity Thru fan openings	2.66 m/s		
Fin Efficiency and coefficient			
Htc to the fins alpha'	47.59 W/m ² .K		
(me)x(lfe)	0.693		
Fin Efficiency Omega	0.866		
Effective fin side Htc	899.9 W/m ² .K	775.1 kcal/h.m ² .K	159 Btu/hr.ft ² .°F
Pressure loss and power consumption			
Bundle loss	9.7 mmWC		
Fan & Plenum loss	0.5 mmWC	Rho based on summer high temp	
Total loss	10.2 mmWC		
Required Fan Power	12.7 KW	17.0 HP	

Sample calculation sheet



Fin Fan Cooler Evaluation		CASE-II	
Geometry (Tubes with radial fins)			
No of fans	2		
Air flow	128.4 kg/s		
Air Inlet T	32.5 °C		
Air Exit T	73.2 °C		
Cp	0.239 kcal/kg.°C		
Duty	4.50 MMKcal/h		
Process f	29.67 kg/s		
Proc Inlet T	146.1 oC		
Proc Out T	65.6 oC		
U process	528.0 kcal/h.m ² .C		
Design U bare	kcal/h.m ² .C		
Types of fins	Extruded		
No of fins/ m	394		
FI OD	mm		
Fin Ht	mm		
Fin thk	mm		
Fin spacing	mm		
Tube OD	mm		
Tube ID	mm		
Tube L	m		
Effective L	m		
Tube pitch	mm		
Total Finned tubes	306		
Rows	5		
Fin Thc W/m.K	208		
Fan dia	m		
Air side calculation			
Geometric factors			
Unfinned surface	0.080 m ² /m	6161	
Finned surface	1.652 m ² /m	ft ²	m ²
Bare external surface	0.080 m ² /m	3206	298
FAR	0.456 Table - 9.2		
Effective Fin ht	0.021 m (Tab-9.3)		
Cooler face area	47.91 m ²		
Flow area between Tubes	21.83 m ²		
Fan Opening area	24.67 m ²		
Dia Based	47.91456		
Total area based	Effective	3937 mm	3930 mm
Overall		end elevation	
Air velocity			
Flow rate standard m ³ /s	104.46	T	15.5 P
Flow rate at fans m ³ /s	110.63	T	32.5 P
Standard Vel Bet Tu	4.79 m/s		
Velocity Thru fan openings	2.31 m/s		
Fin Efficiency and coefficient			
Htc to the fins alpha'	43.56 W/m ² K		
(me)x(lfe)	0.663		
Fin Efficiency Omega	0.875		
Effective fin side Htc	832.5 W/m ² K	717.0 kcal/h.m ² .K	147 Btu/hr.ft ² .°F
0.204813			
Pressure loss and power consumption			
Bundle loss	7.7 mmWC		
Fan & Plenum loss	0.4 mmWC	Rho based on summer high temp	
Total loss	8.1 mmWC		
Required Fan Power	8.8 KW	11.8 HP	

Fin Fan Cooler Evaluation		CASE-III	
Geometry (Tubes with radial fins)			
No of fans	2		
Air flow	125.7 kg/s		
Air Inlet T	31.9 °C		
Air Exit T	73.5 °C		
Cp	0.239 kcal/kg.°C		
Duty	4.50 MMKcal/h		
Process f	29.67 kg/s		
Proc Inlet T	146.1 oC		
Proc Out T	65.6 oC		
U process	528.0 kcal/h.m ² .C		
Design U bare	kcal/h.m ² .C		
Types of fins	Extruded		
No of fins/ m	394		
FI OD	mm		
Fin Ht	mm		
Fin thk	mm		
Fin spacing	mm		
Tube OD	mm		
Tube ID	mm		
Tube L	m		
Effective L	m		
Tube pitch	mm		
Total Finned tubes	306		
Rows	5		
Fin Thc W/m.K	208		
Fan dia	m		
Air side calculation			
Geometric factors			
Unfinned surface	0.080 m ² /m	6161	
Finned surface	1.652 m ² /m	ft ²	m ²
Bare external surface	0.080 m ² /m	3206	298
FAR	0.456 Table - 9.2		
Effective Fin ht	0.021 m (Tab-9.3)		
Cooler face area	47.91 m ²		
Flow area between Tubes	21.83 m ²		
Fan Opening area	24.67 m ²		
Dia Based	47.91456		
Total area based	Effective	3937 mm	3930 mm
Overall		end elevation	
Air velocity			
Flow rate standard m ³ /s	102.22	T	15.5 P
Flow rate at fans m ³ /s	108.05	T	31.9 P
Standard Vel Bet Tu	4.68 m/s		
Velocity Thru fan openings	2.26 m/s		
Fin Efficiency and coefficient			
Htc to the fins alpha'	42.92 W/m ² K		
(me)x(lfe)	0.658		
Fin Efficiency Omega	0.877		
Effective fin side Htc	821.7 W/m ² K	707.7 kcal/h.m ² .K	145 Btu/hr.ft ² .°F
0.204813			
Pressure loss and power consumption			
Bundle loss	7.5 mmWC		
Fan & Plenum loss	0.3 mmWC	Rho based on summer high temp	
Total loss	7.8 mmWC		
Required Fan Power	8.3 KW	11.1 HP	



Savings in power through VSD on fin fan cooler

ASD Eff	95%	Temp	Power Cons	Total Po Cons
No of months	No of Hrs/day			
2	24	35.8	28.8	41433
2	24	32.5	19.9	29088
2	24	31.9	18.7	27341
2	24	23.7	9.0	13461
2	24	22.1	8.0	11740
2	24	19.6	6.7	9826
			Total KW/Yr	111324
Actual power Consumption			60.0	
			Total KW/Yr	527037
\$/MW	19.36			
			Saving KW/Yr	409853
			Saving \$/Y	7934.76

- The pay back for such replacement is less than a year however depending on cost of power it may go up to 3 – 3.5 years.

Low level heat recovery

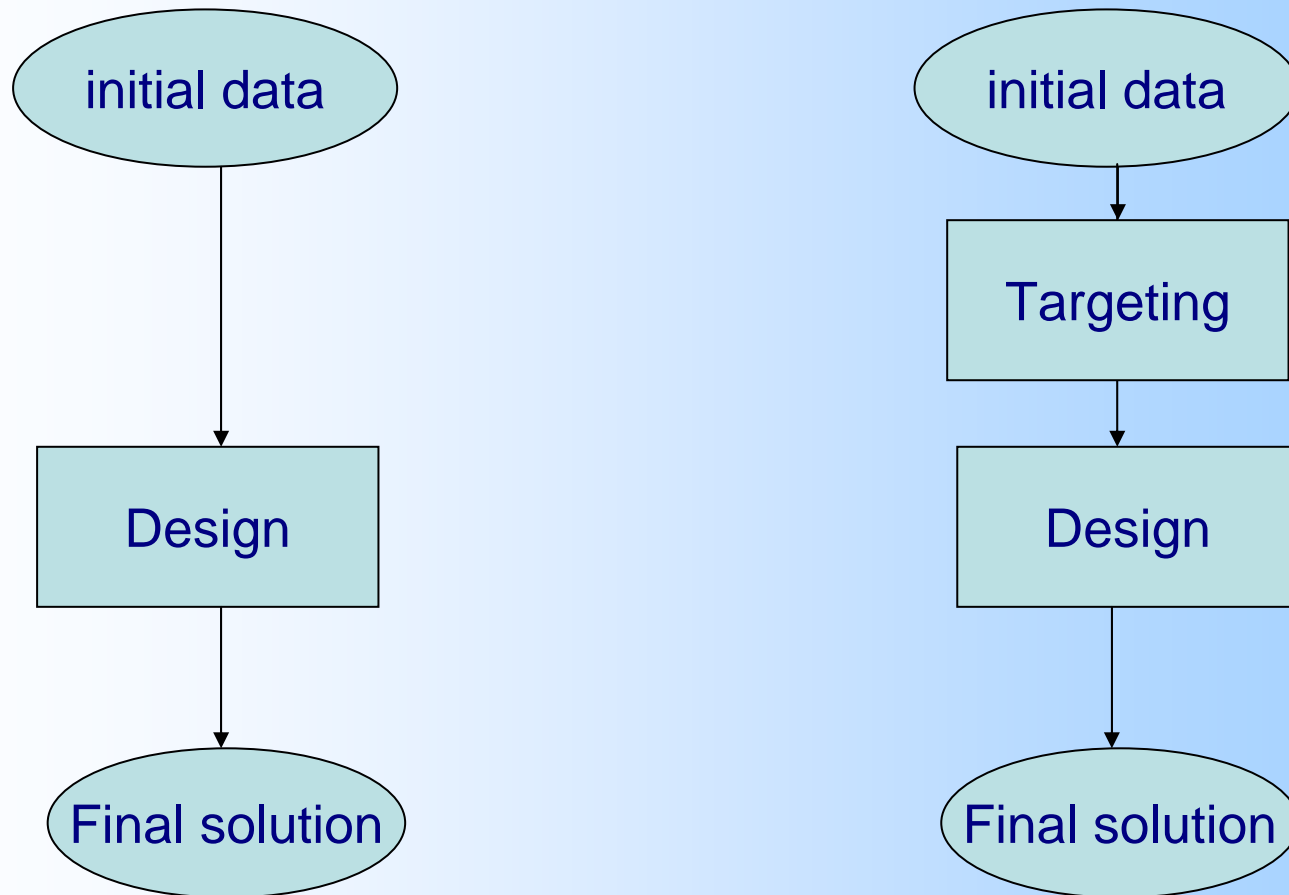


- Explore possibility of recovering low level heat
 - Useful for BFW heating
 - Can be used for vapor absorption chiller to produce cold for refrigeration
 - Trigeneration – combined heat, cooling and power



- Pinch technology
 - Heat exchange systems
 - Separation systems
 - Process changes

Pinch technology - approach

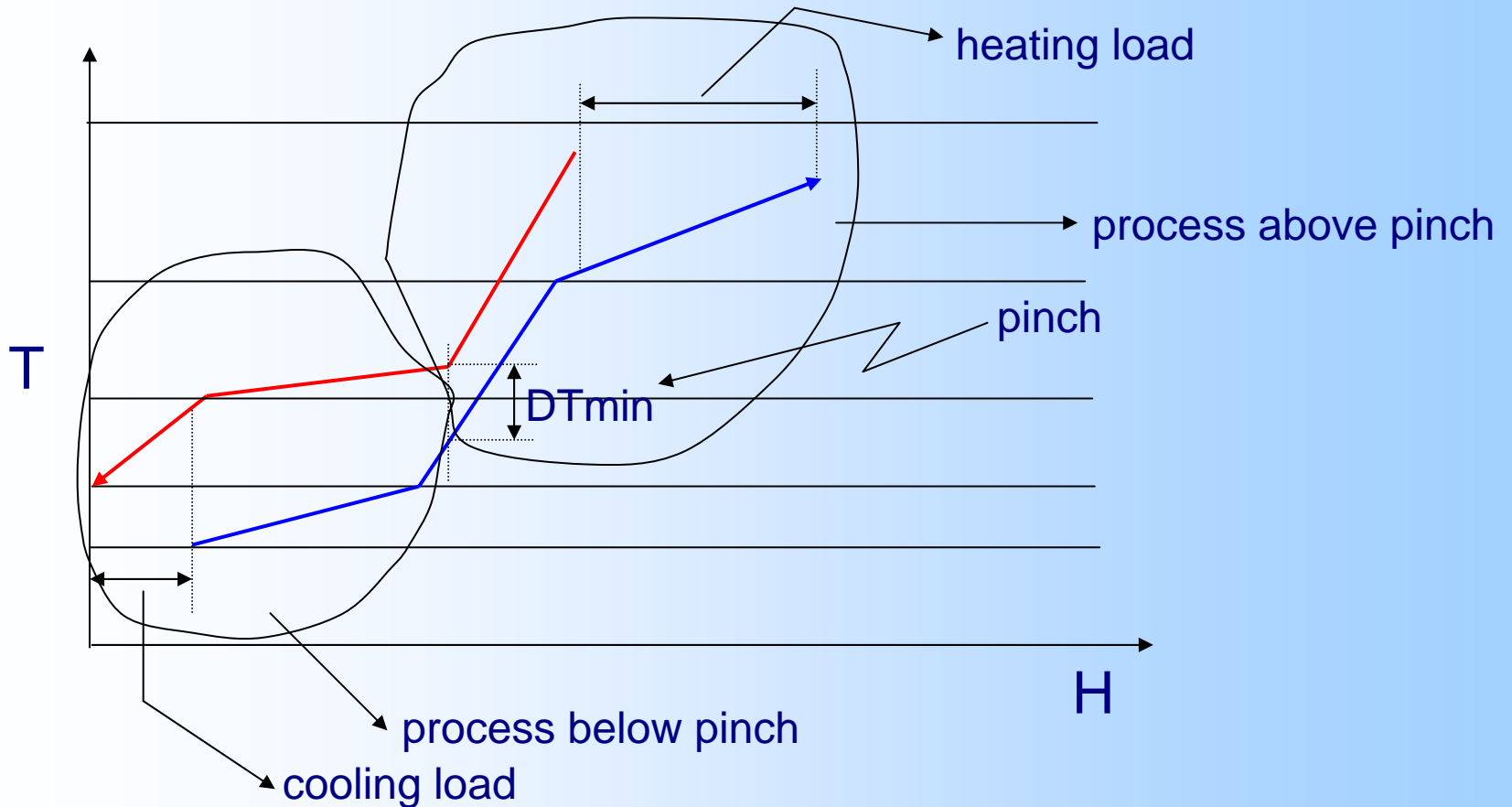


Pinch analysis heat exchange systems

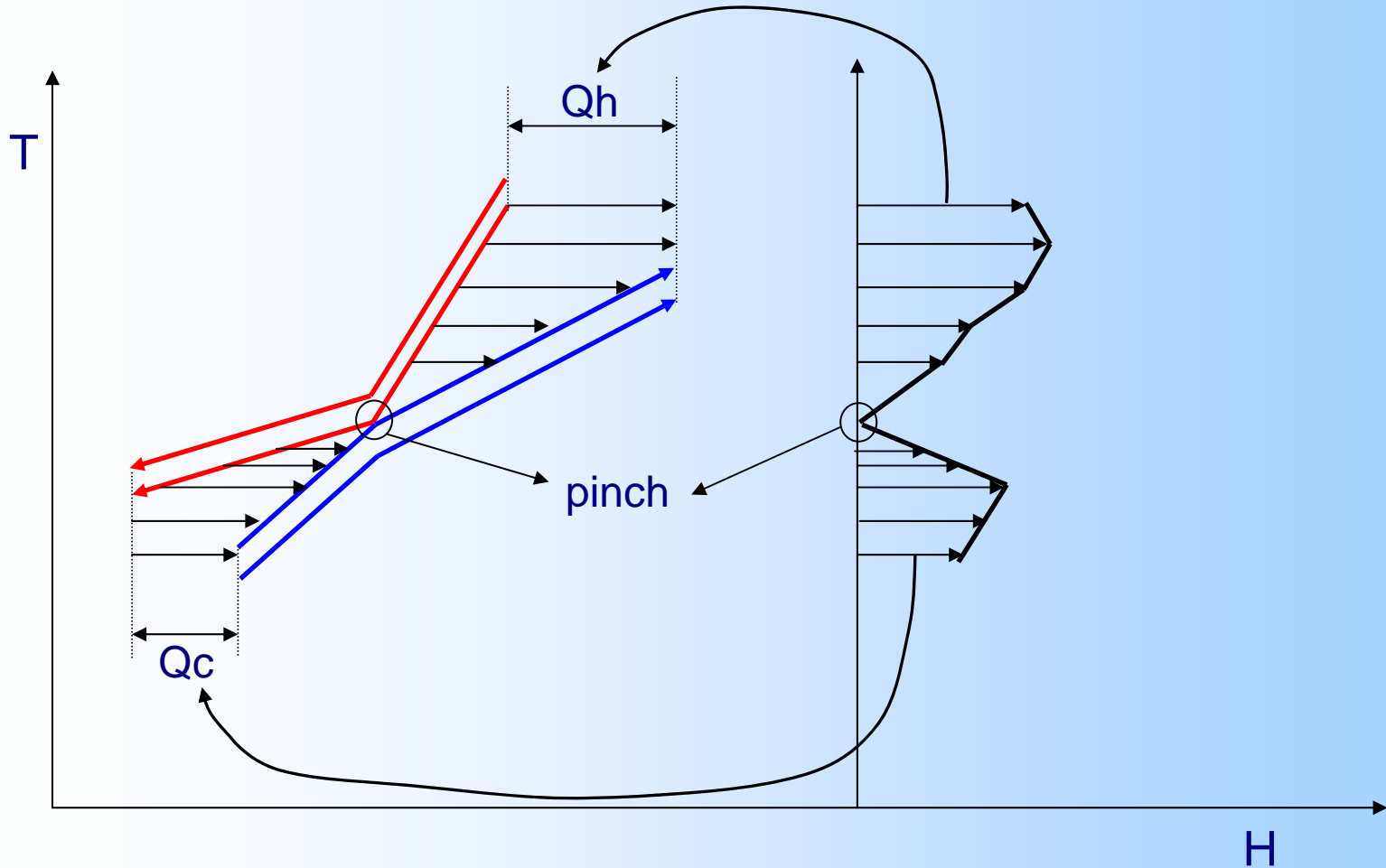


- Collect all heat sources and heat sinks of process
- Represent them on a common platform of resource and driving force
- In heat exchange system it is temp vs enthalpy change diagram, in mass exchange it is conc vs mass change

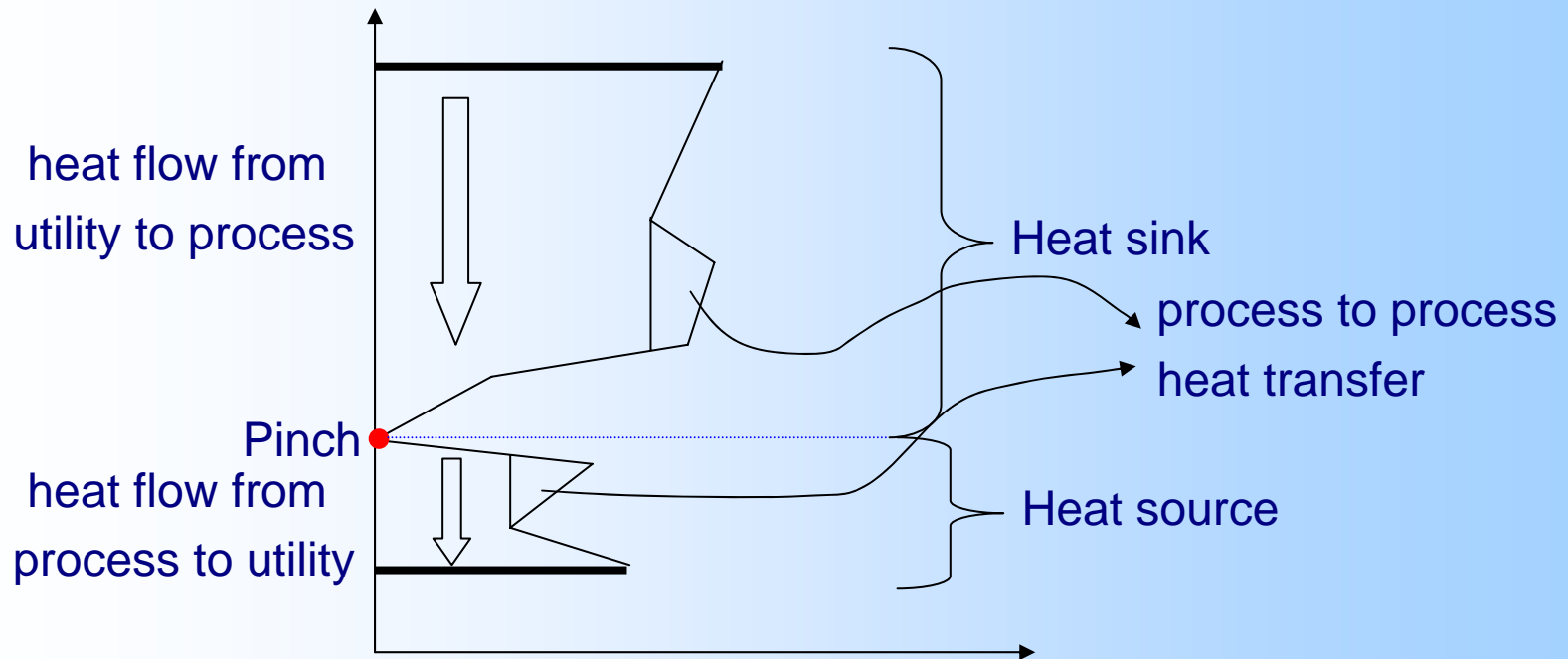
HEN - Composite curves



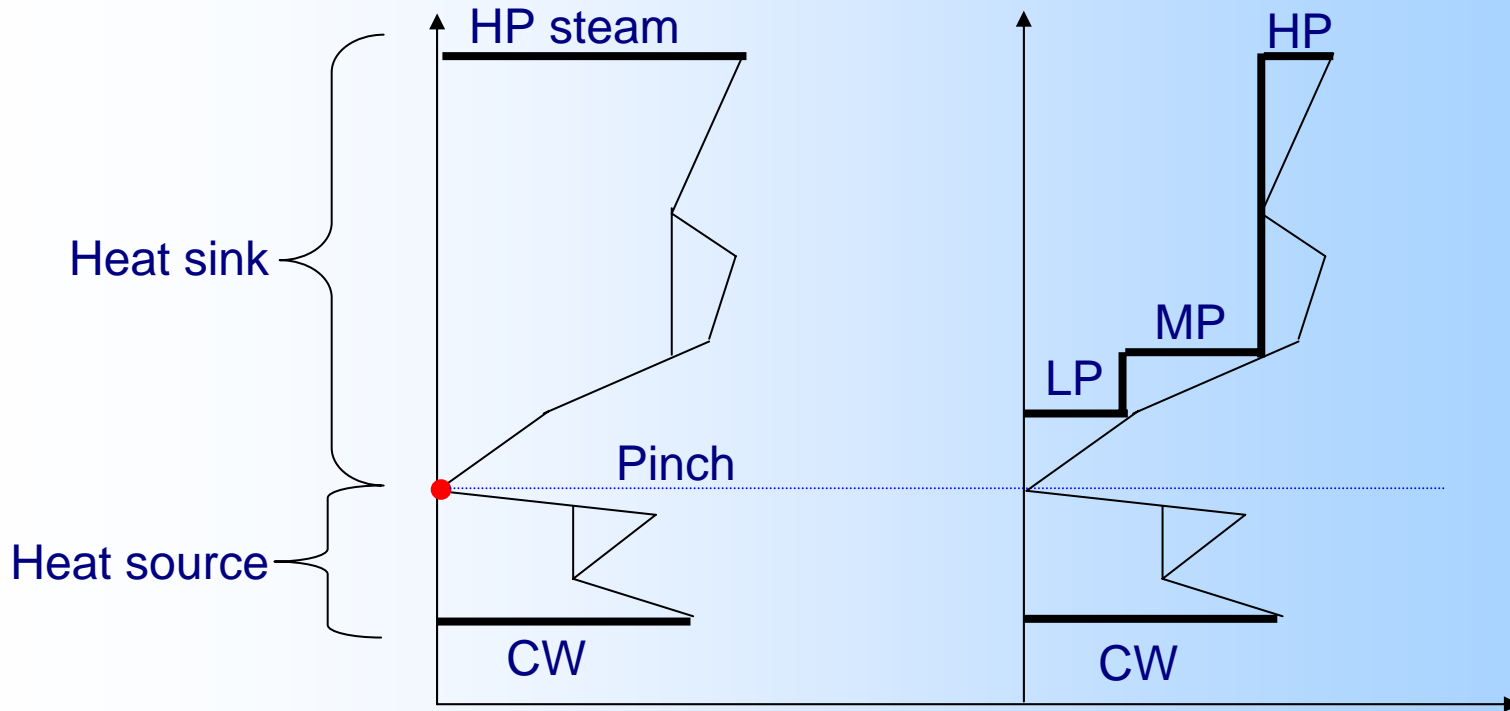
Grand composite curve



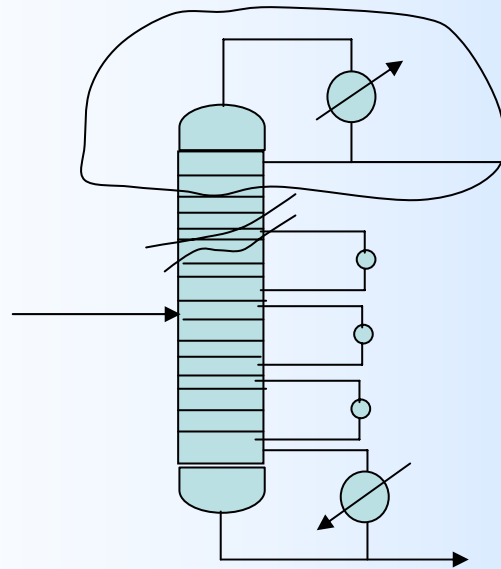
Grand composite curve



Grand composite curve



Separation system – distillation column



D_L, D_H

- Operating line

$$VY_L - LX_L = D_L$$

$$VY_H - LX_H = D_H$$

- Equilibrium line

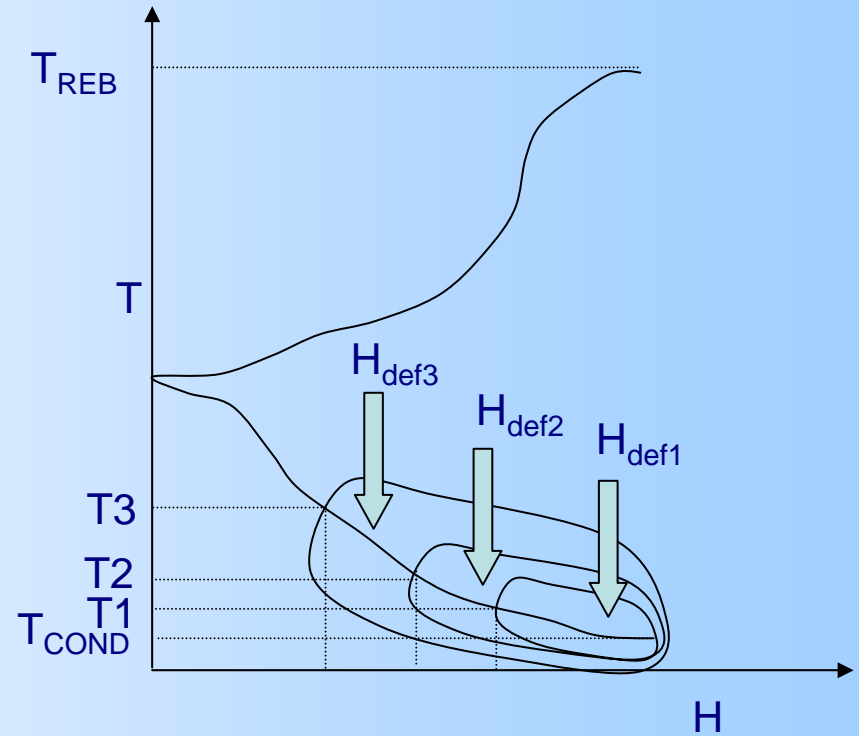
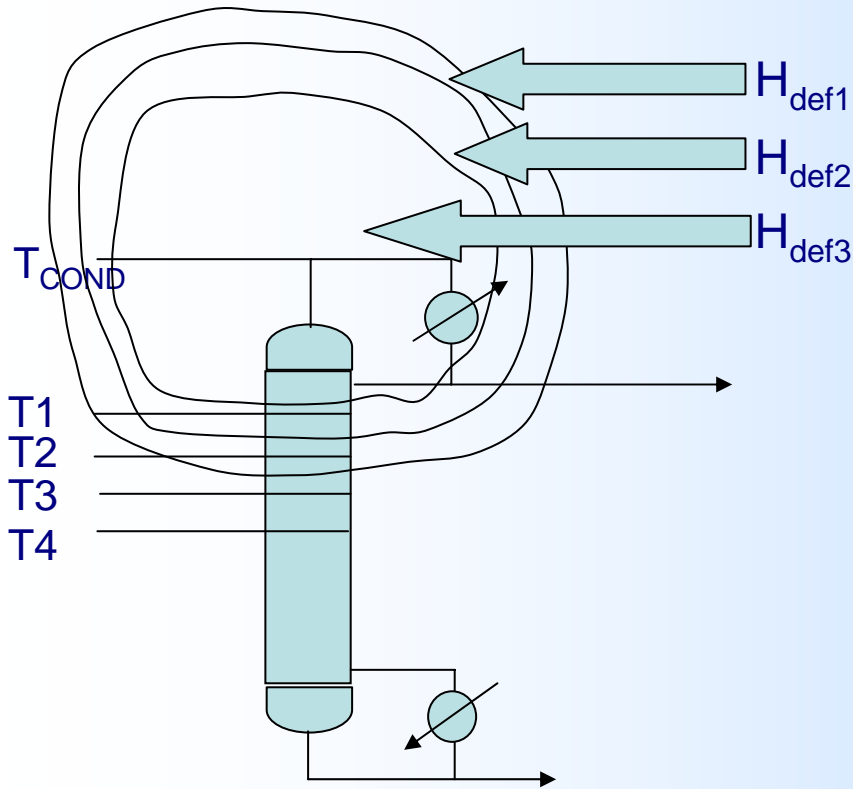
$$\left. \begin{array}{l} Y_L^*, X_L^* \\ Y_H^*, X_H^* \end{array} \right\} \text{From simulation}$$

$$V_{\min} Y_L^* - L_{\min} X_L^* = D_L$$

$$V_{\min} Y_H^* - L_{\min} X_H^* = D_H$$

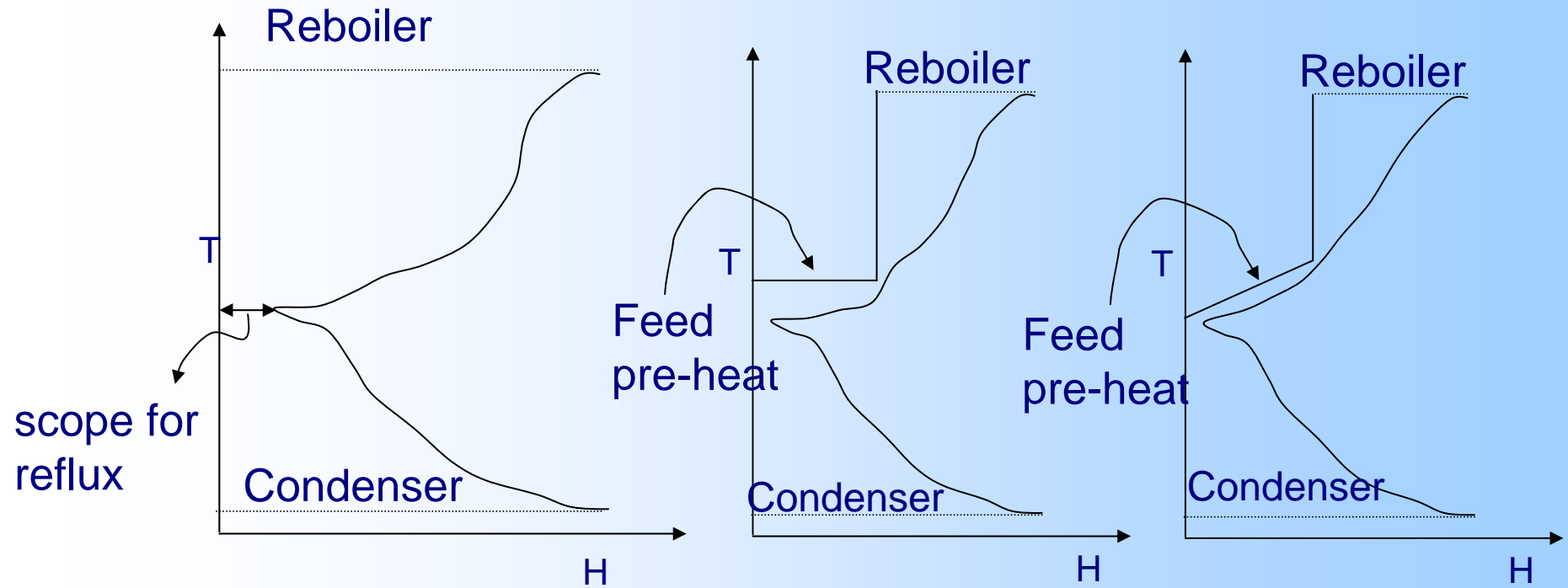
Two simultaneous equations to solve
Evaluate $V_{\min} \cdot L_{\min}$ and enthalpy deficit

Separation system – distillation column



Column temperature – enthalpy profile

Distillation column – Energy analysis



Process changes



- Recycle loops
- Feed variation
- Condenser re-boiler integration
- Heat engine / heat pump placement and sizing
- Multiple feed cases etc

Utility systems



- Utility boilers
 - Efficiency estimations and improvement
 - $F = a + bS + cS^2$
- Steam turbine
 - Performance analysis
- Gas turbines
 - Performance analysis
 - $F = a + bP + cP^2 + dT + eT^2$
- HRSG
 - Performance analysis
 - $S = a + bF + cF^2 + dT + eT^2$
- Insulation losses
- Steam trap

Steam loss through trap



- Steam as high as 15-20% of leaving a boiler lost via leaking traps
- With best steam trap and proactive steam trap maintenance programme can reduce loss to less than 1%
- A single leaking trap (100psig with 1/8-in. [3mm] orifice) can Squander more than \$2000/yr

Steam trap distribution



Total traps by pressure, %	Total traps by pressure/ condensate- load, %
8% 30 kg/cm² (g) & above (High-Pressure)	<1% Large condensate load (>1500 kg/h) 1% Medium condensate load (250-1500 kg/h) 7% Small condensate load (< 250kg/h)
12% 7 to 30 kg/cm² (g) (Moderate-pressure)	<1% Large condensate load (>1000 kg/h) 2% Medium condensate load (100-1000 kg/h) 10% Small condensate load (< 100kg/h)
80% 2.5 to 7 kg/cm² (g) (Low-Pressure)	<1% Large condensate load (>500 kg/h) 2% Medium condensate load (50-500 kg/h) 78% Small condensate load (< 50kg/h)

EIL developed steam trap



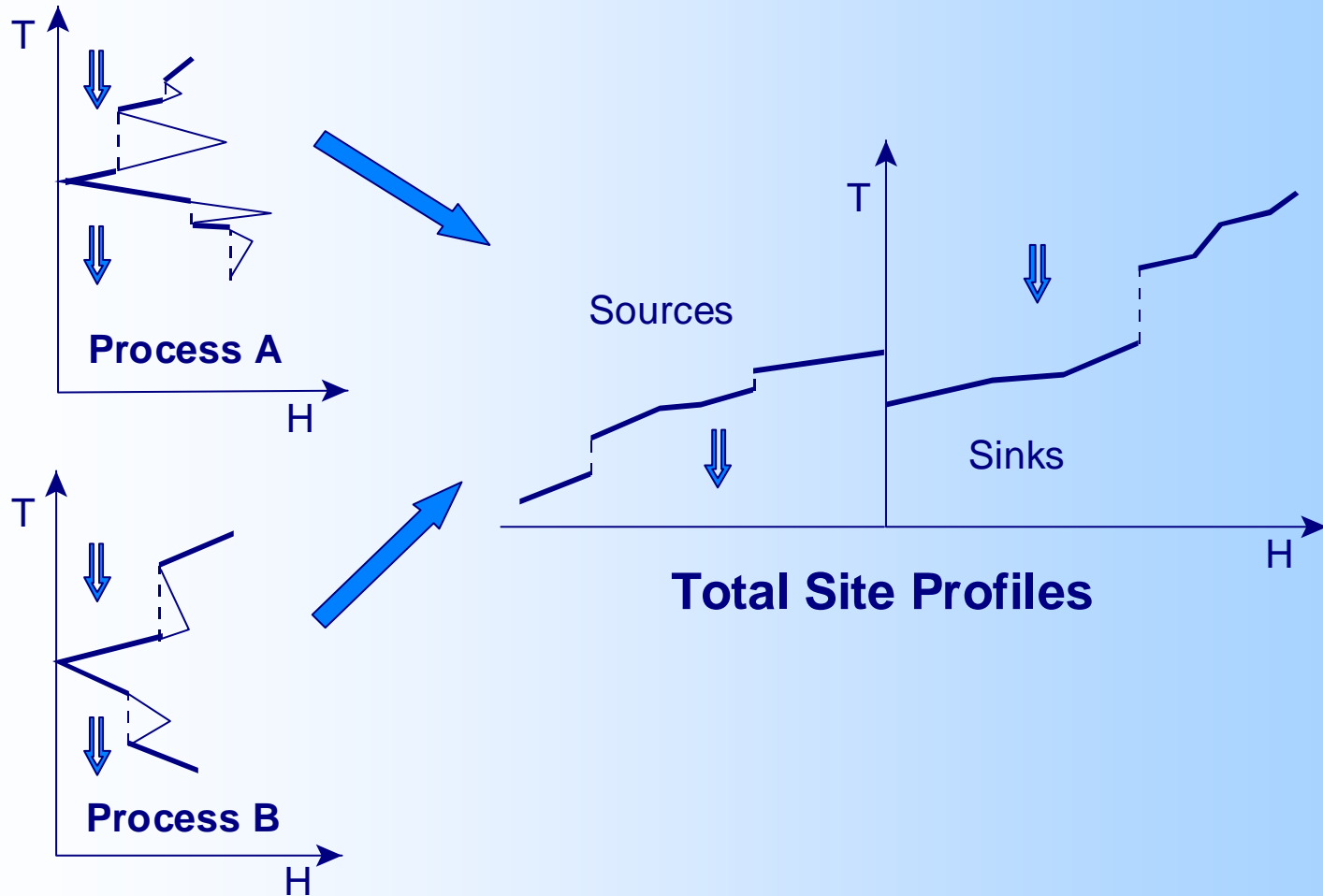
- Indigenous design
- High reliability
- High energy saving
- Field Trials : 2yrs at R&D pilot plant
- Commercial testing :
 - One year at CPCL, Chennai
 - Six months at IOCL, Mathura
- Performance wise better than other traps
- Zero live steam loss up to 3.5 kg/cm²
- Can save Rs 183 crores every year for refineries having estimated 100,000 traps

Integrated analysis

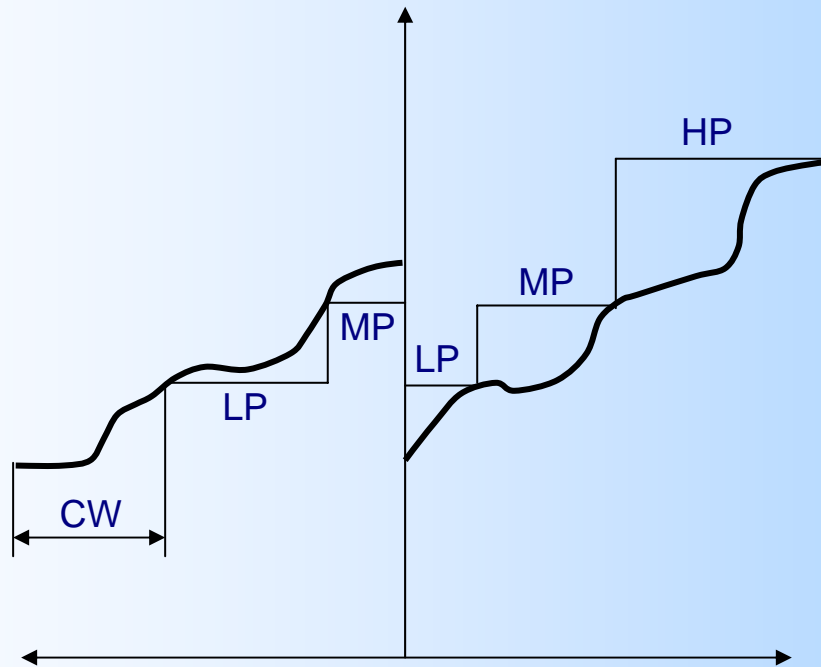


- Total site analysis – Pinch approach
 - Utility network – CHP system
 - Optimizing steam mains
 - Cogeneration targeting
 - Path level / top level analysis
 - Hydrogen networks
 - Water and waste water minimization

Total site profiles

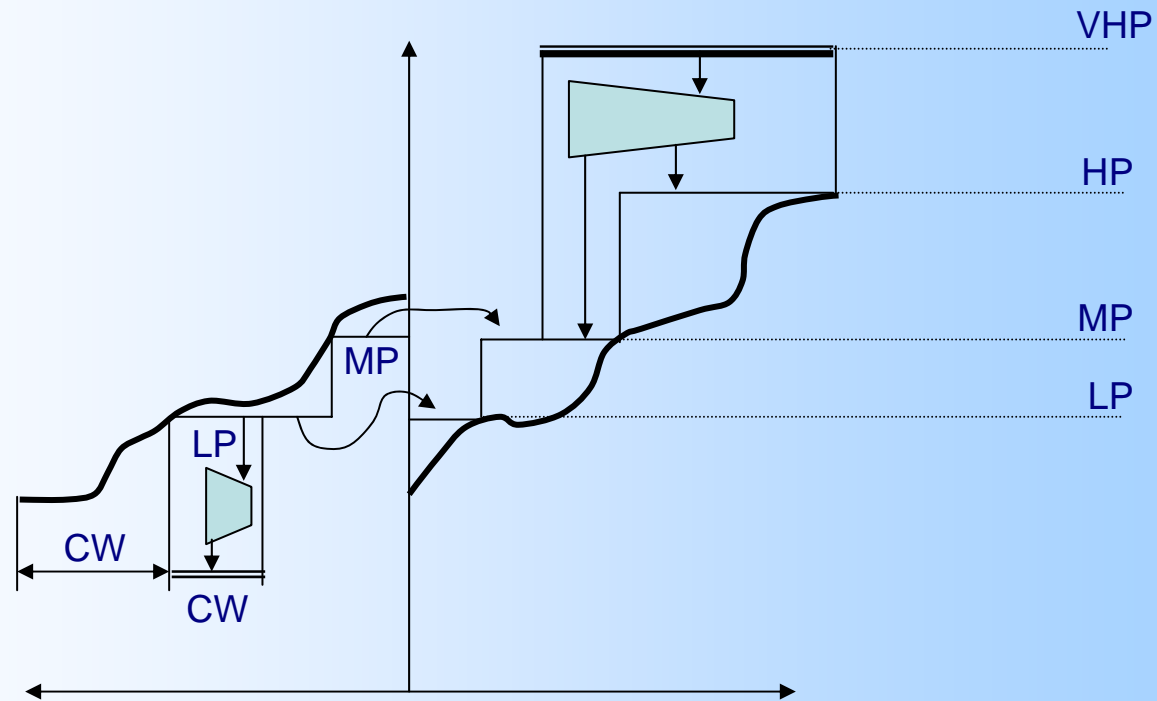


Total site profiles



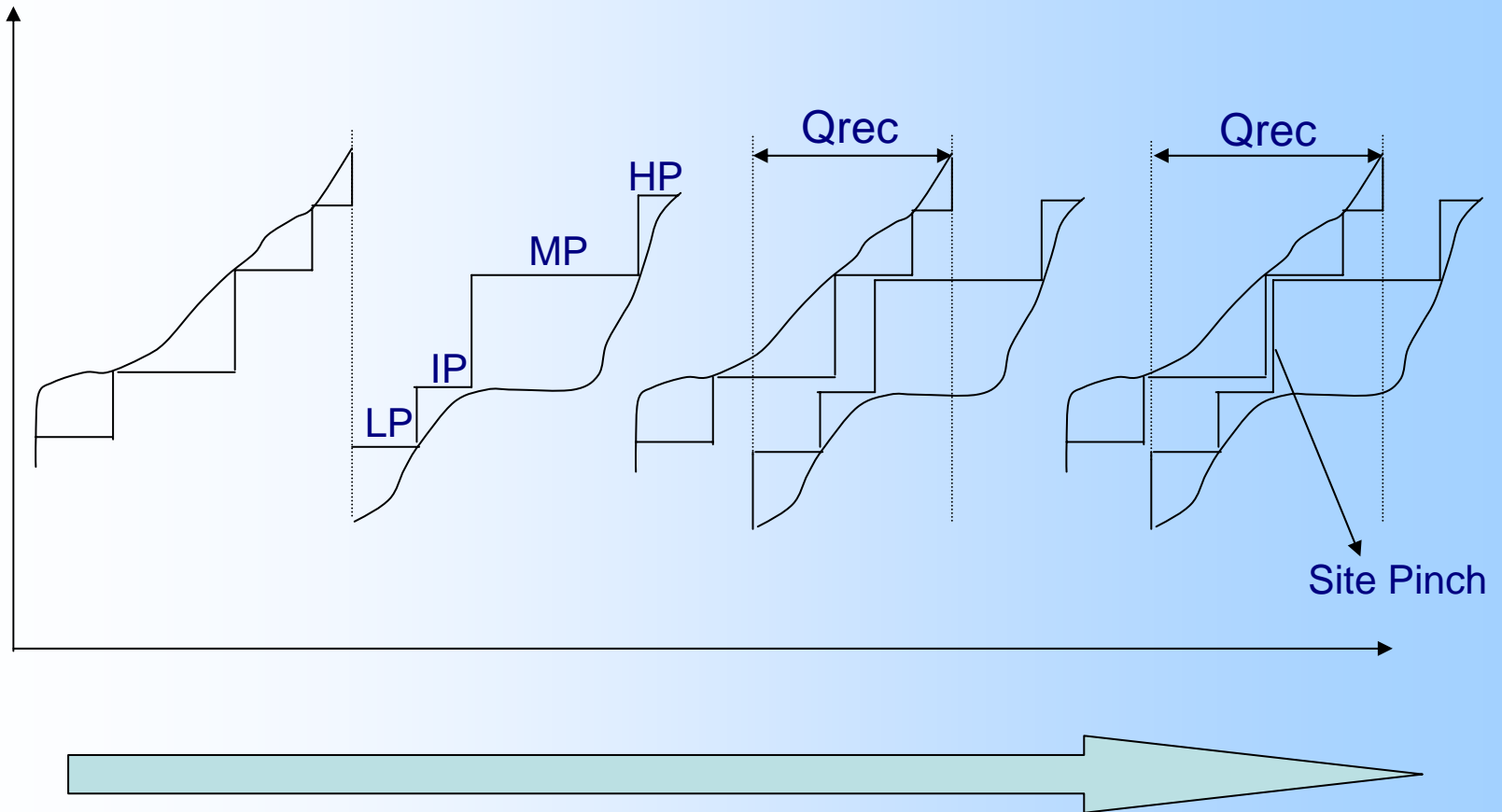
Set targets for steam load

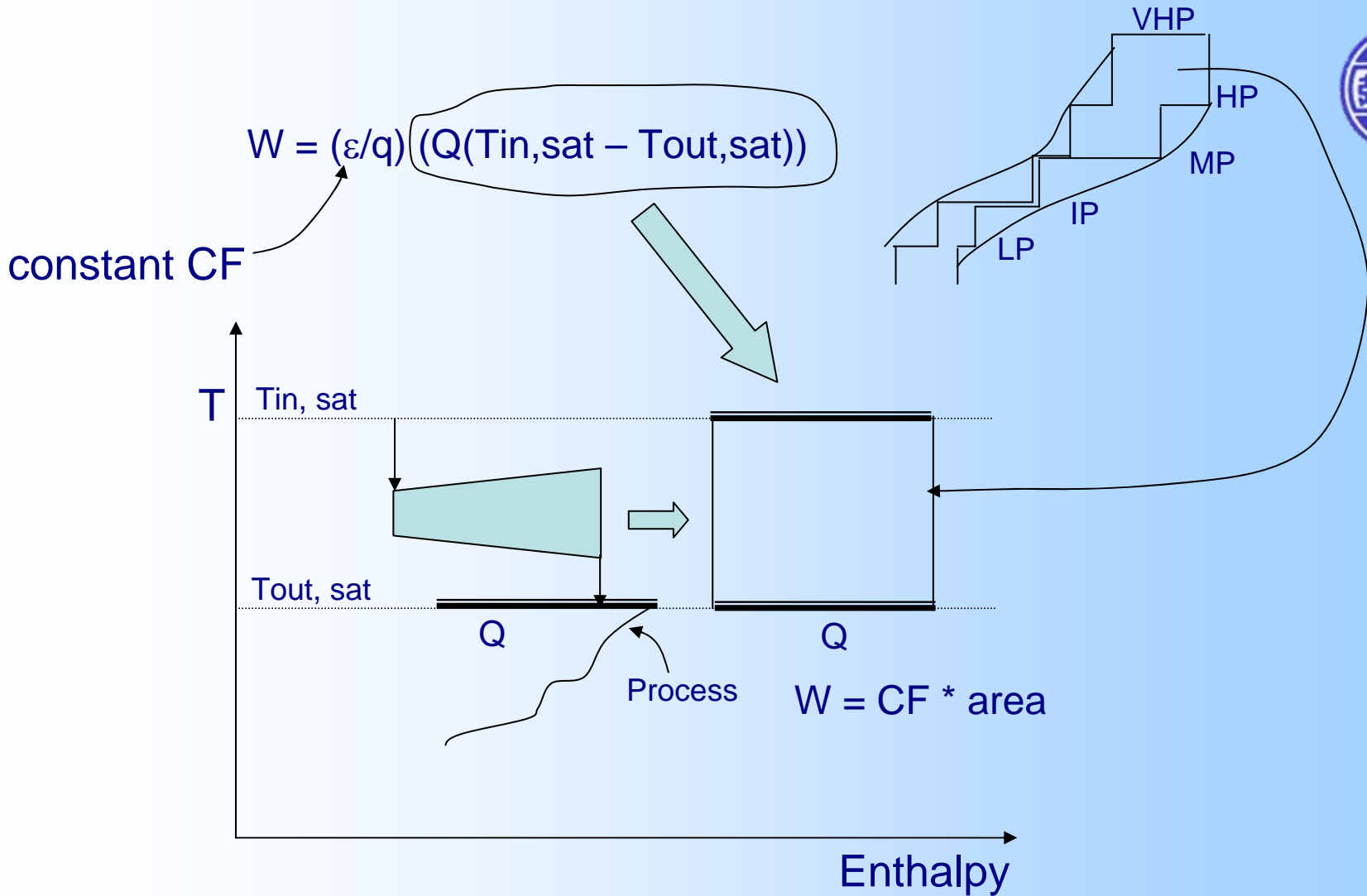
Total site profiles



- Improve total site utility systems
- Plan future infrastructure investment

Procedure



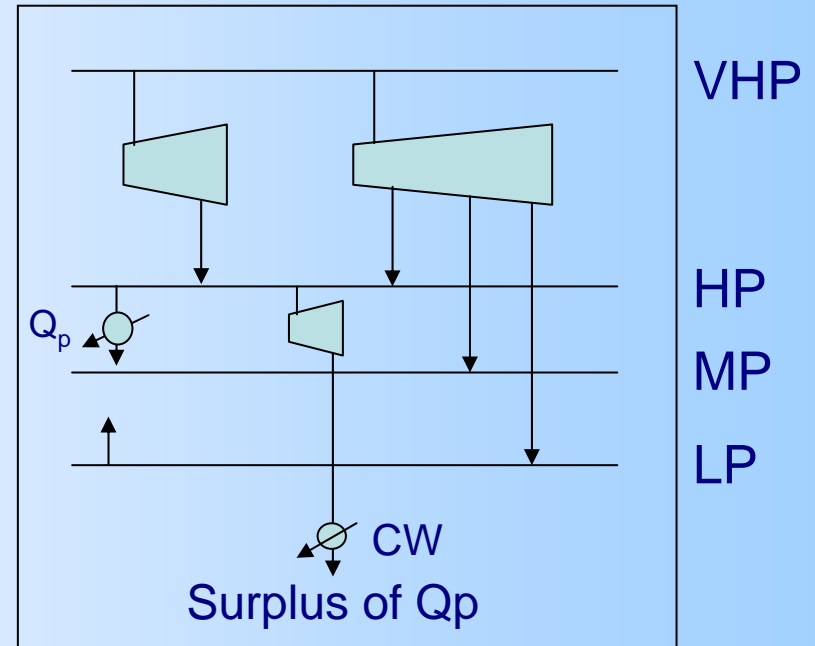
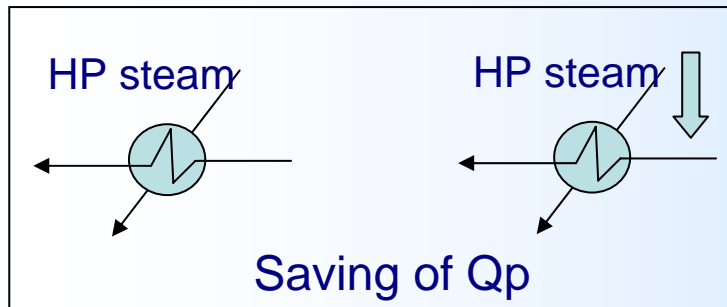


Utility network - CHP



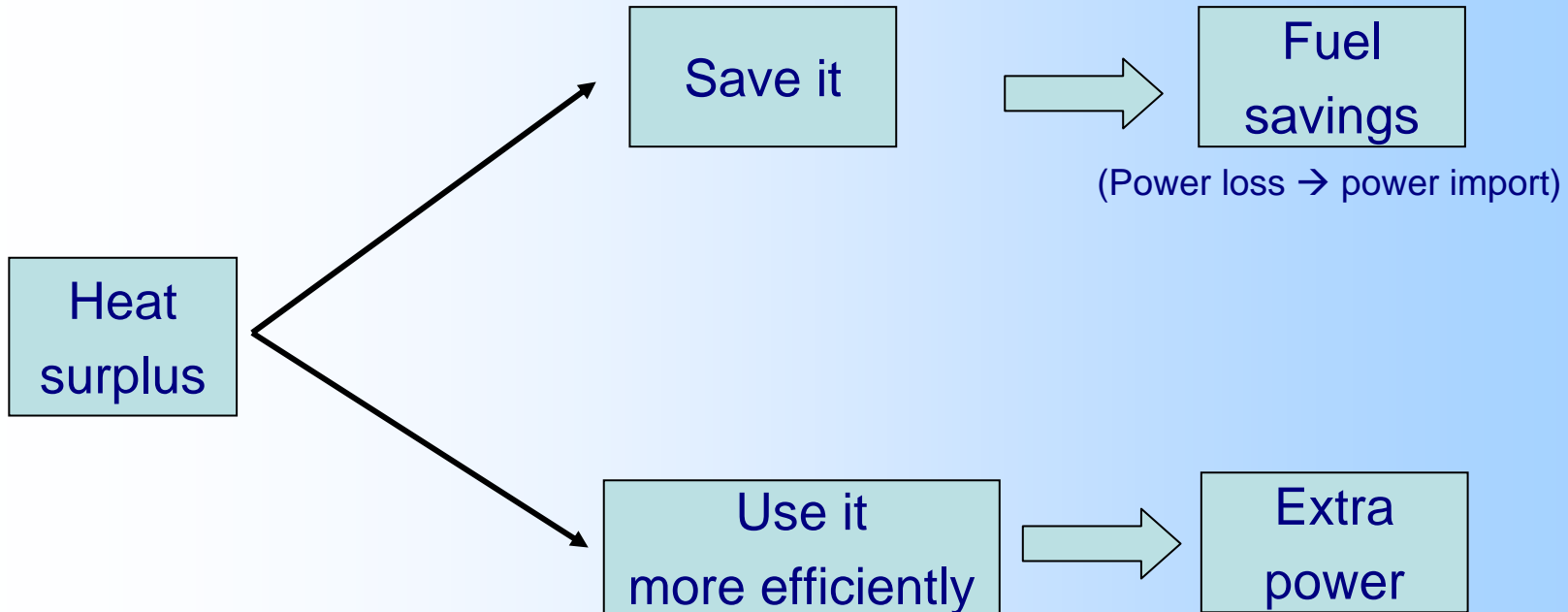
- Understanding interaction between various components of process and utility.
- Identify opportunity for cost reduction through efficiency improvement.
- Identify load shaping strategy
- Evaluating various energy conservation projects for fuel saving by plugging them in the CHP model.

Path level analysis



Implications of energy savings on utility systems

Options for surplus usage

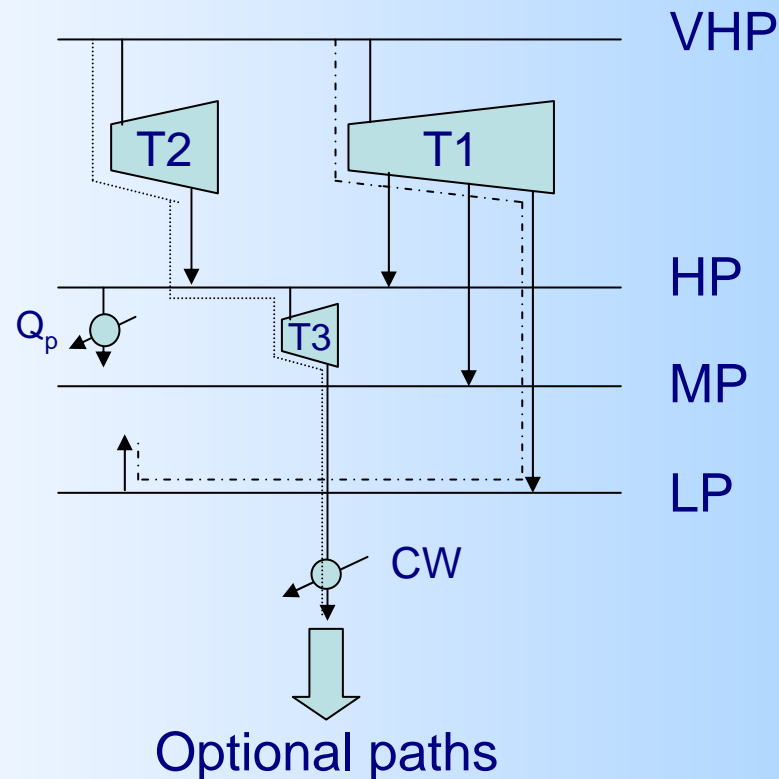


Which option is more economic ?

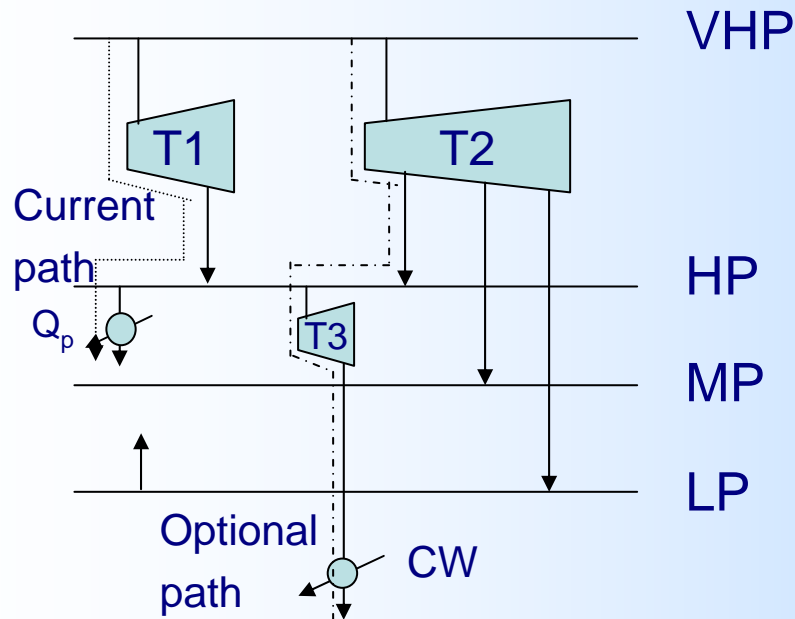
Implications of surplus Q_p steam at any steam level
surplus Q_p means surplus VHP



How do we use the surplus more efficiently?
identify heat-flow paths to use surplus steam



Illustration



$$\eta_{\text{current}} = 0.042$$

$$\eta_{\text{optional}} = 0.359$$

$$\eta_{\text{import power}} = 0.24$$

$$\eta_{\text{current}} < \eta_{\text{import power}} < \eta_{\text{optional}}$$

- Step 1 Exhaust the optional path by shifting surplus from current path
- Step 2 Convert any other further surplus on current path to fuel savings and import power

Water and waste water minimization



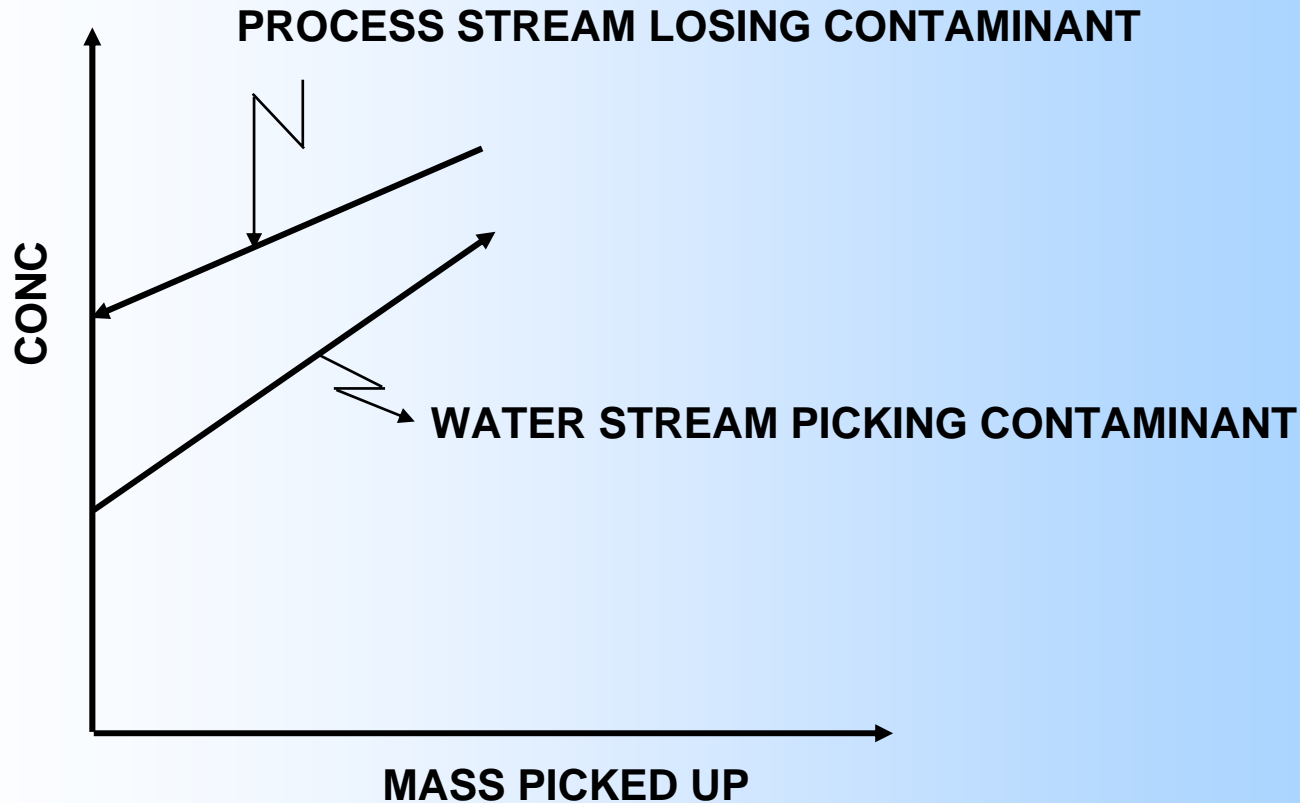
- General approach
 - Process changes
 - Improved effluent treatment
 - Intra & inter process water reuse / recycle

Water pinch analysis

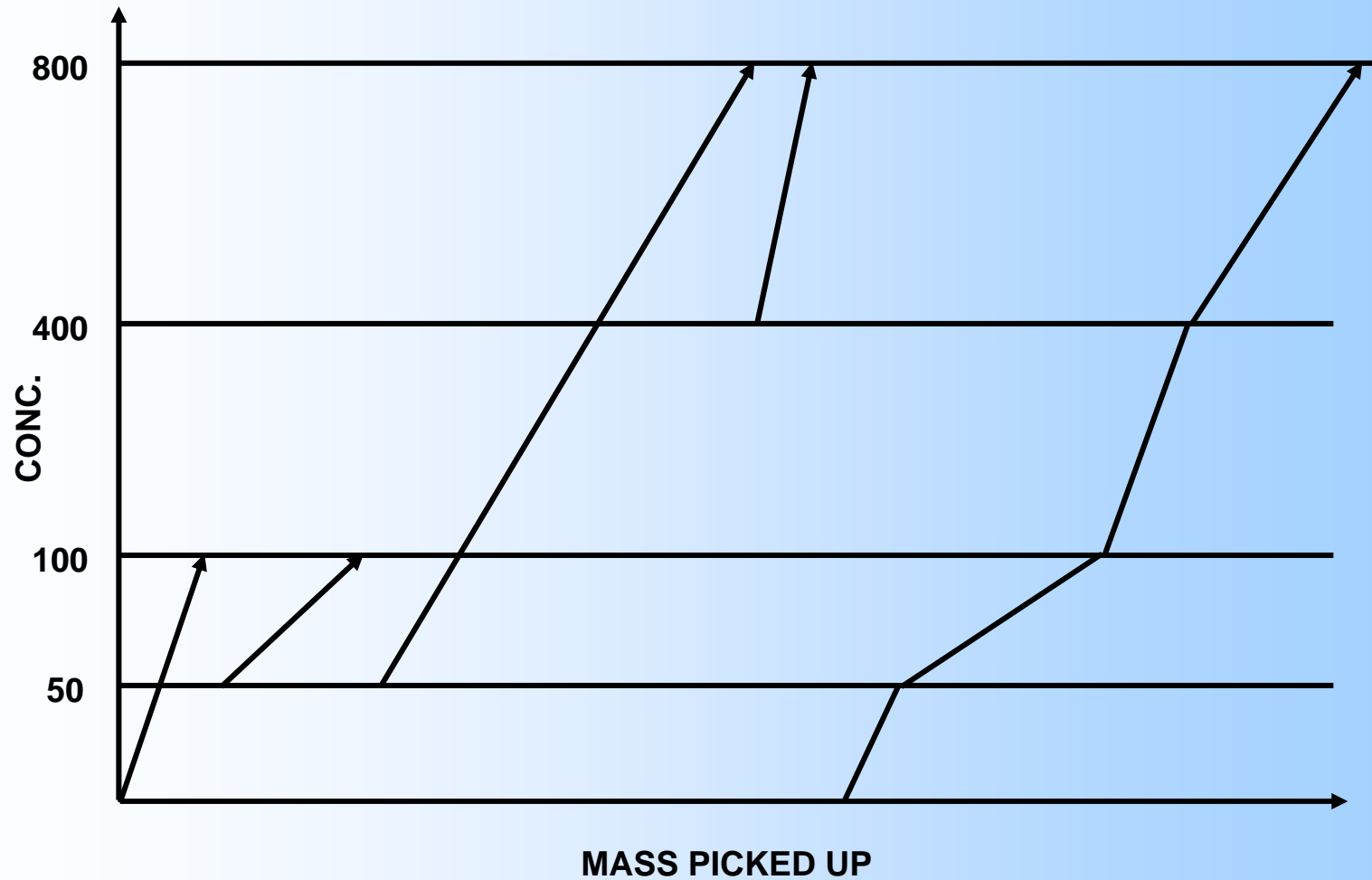


- Waste water is characterized by vol. and load of the contaminant
- Water consuming operations are represented graphically on conc. Vs. mass picked up diagram
- The techniques are well tested for thermal networks and similar principals have been extended for mass exchange networks

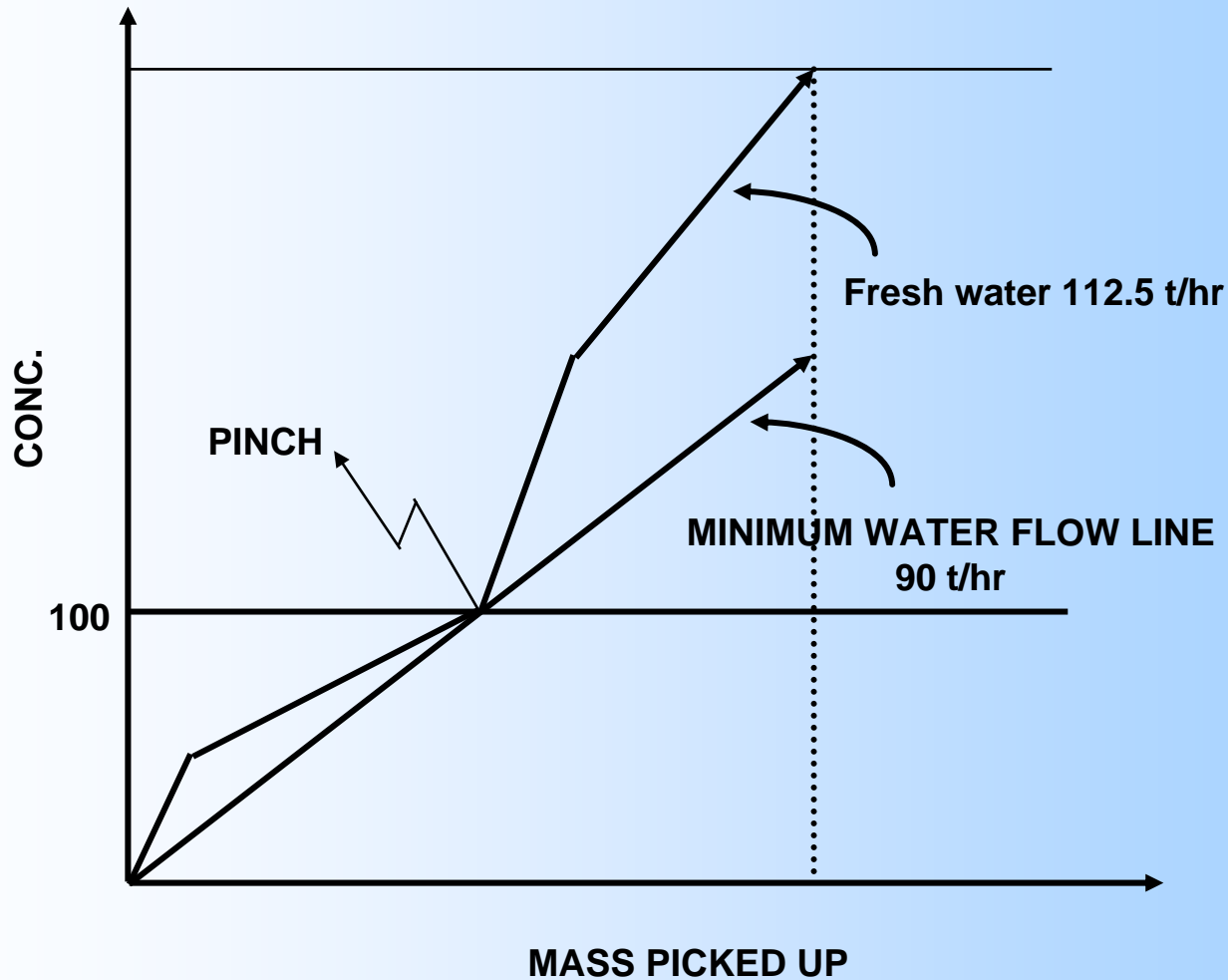
Water consuming operation



Water composite curves



Minimum water targets

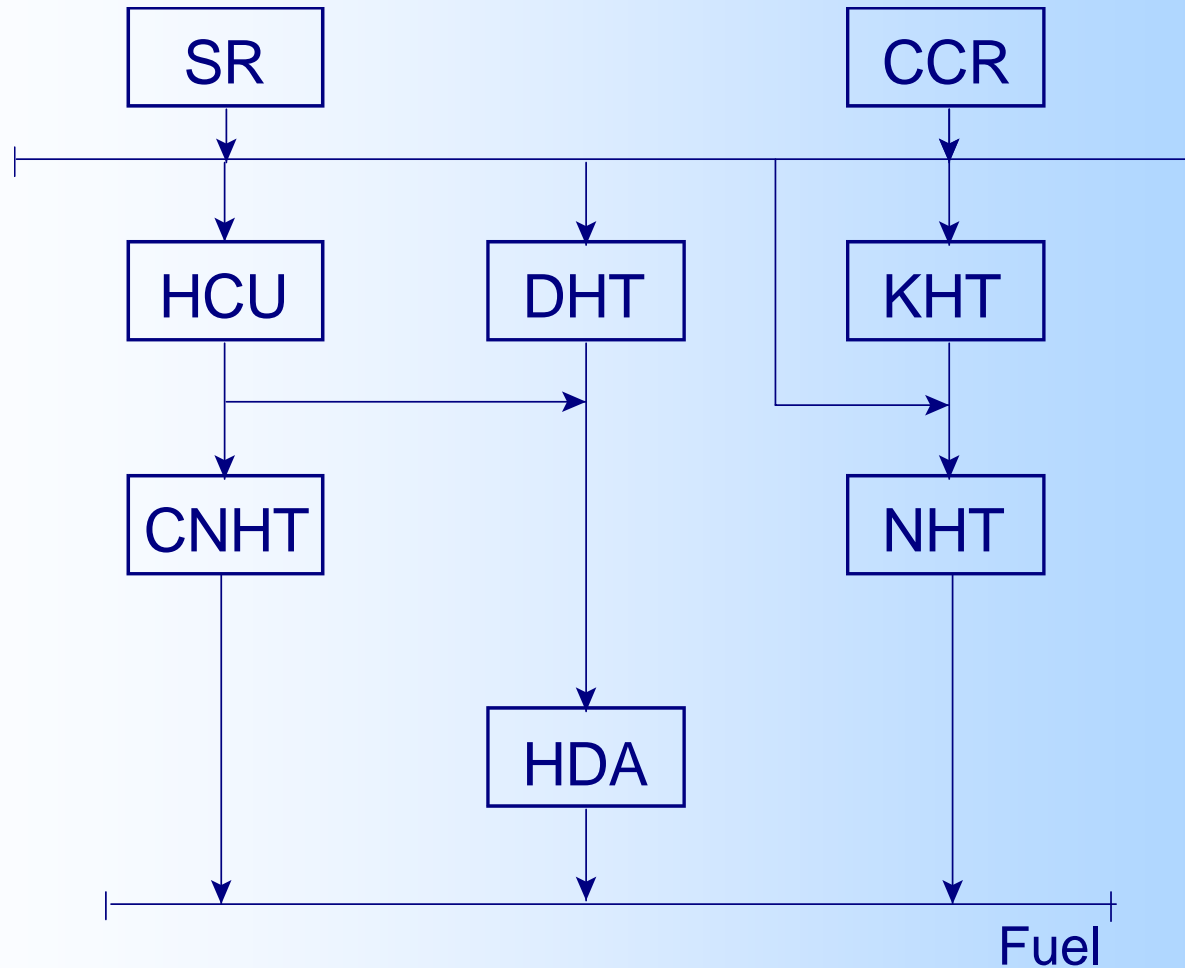


Hydrogen management



- Objectives
 - Hydrogen network optimization
 - Hydrogen purification
 - Process modifications
- Hydrogen network
 - Hydrogen consumers
 - Hydrogen producers
 - Purification operations

Typical hydrogen distribution system

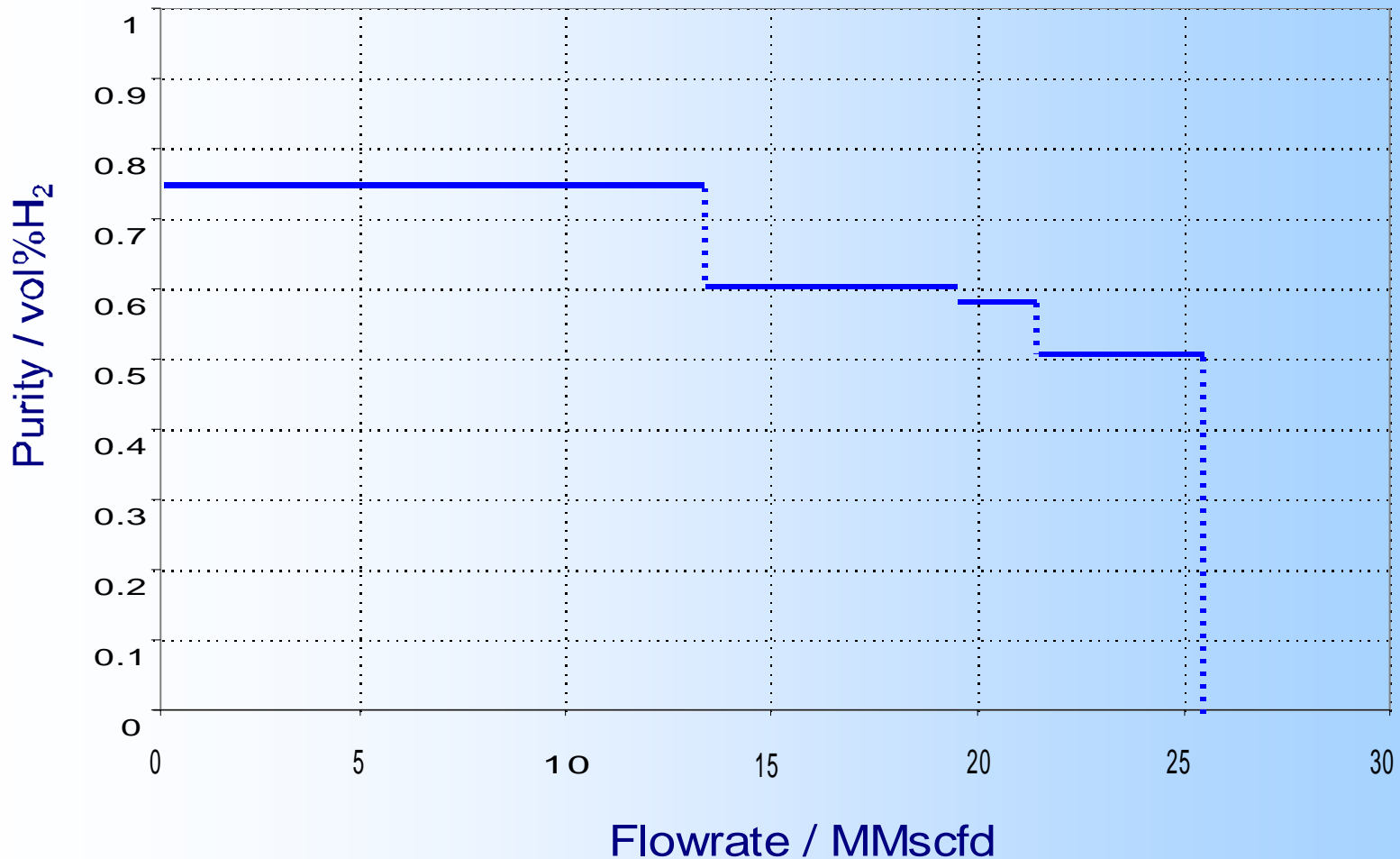


Analysis methodology

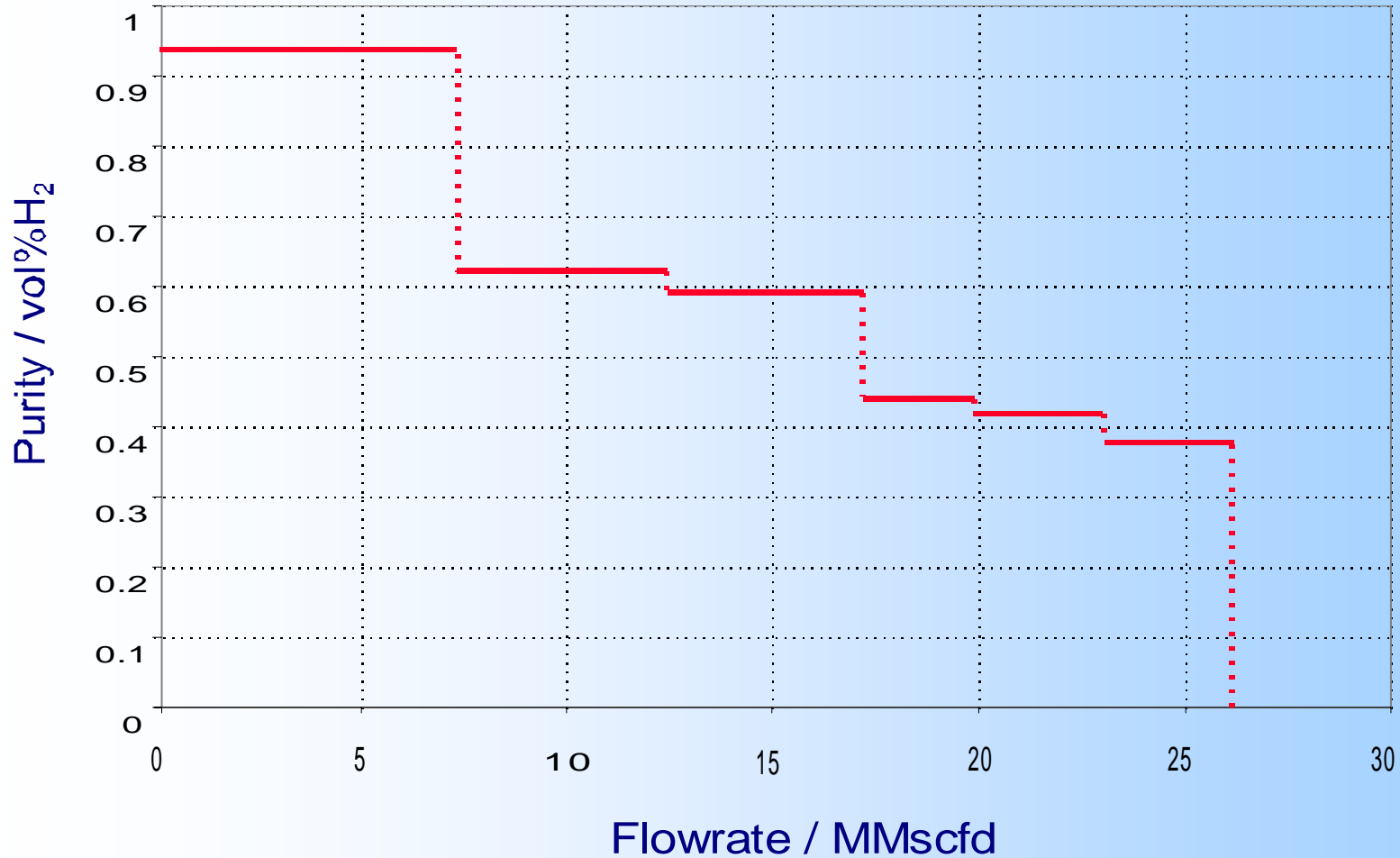


- Similar to heat recovery networks
- All sources and sinks of hydrogen are identified
 - sources are SR, CCR, imports etc
 - sinks are hydro-processing units, hydro-cracker etc
- Composites of demand and supply are generated
 - flow rate Vs. purity
- Targets for minimum hydrogen utility are established
- Pinch techniques are used to achieve the targets

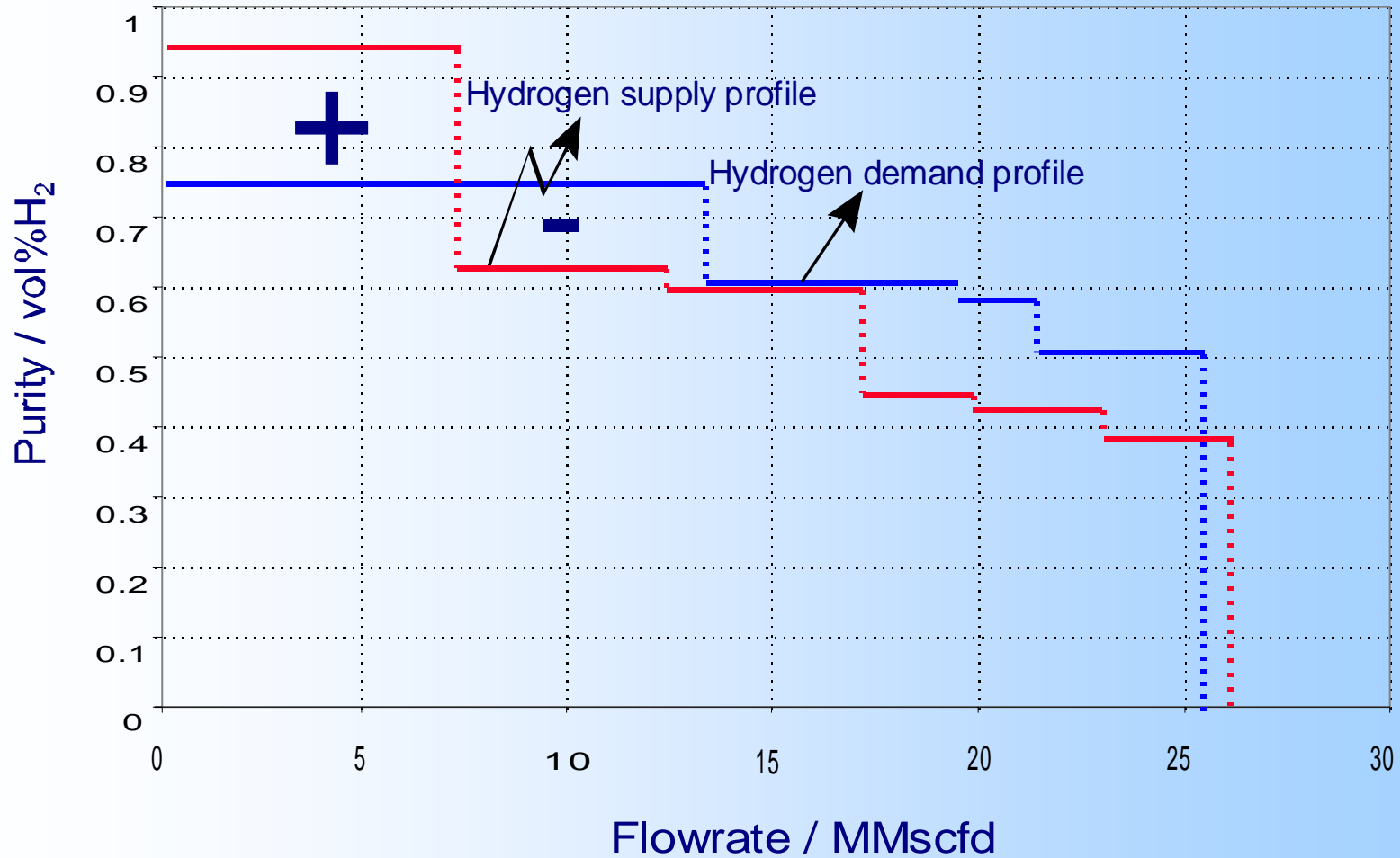
Purity Vs flow rate demand profile



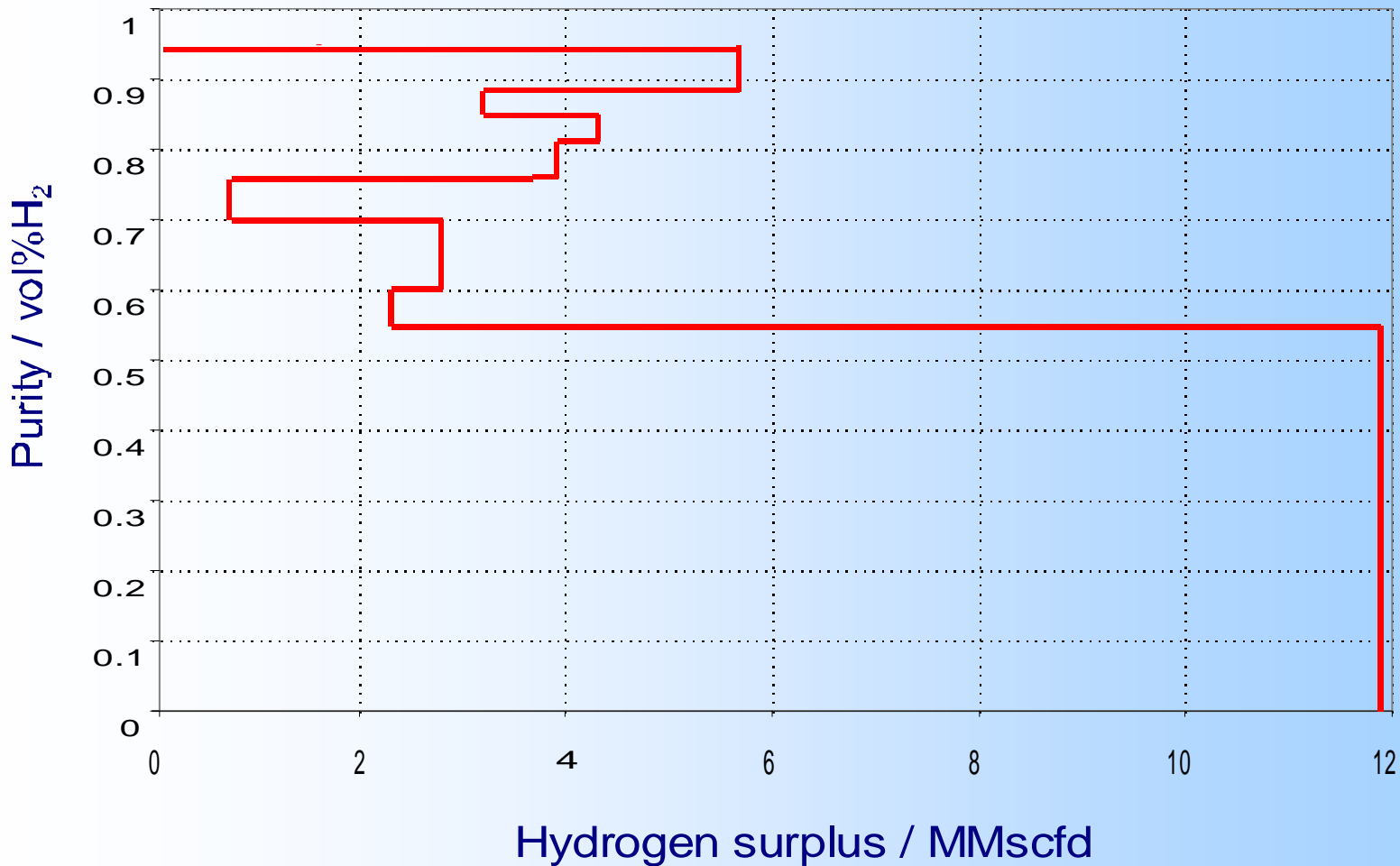
Purity Vs flow rate supply profile



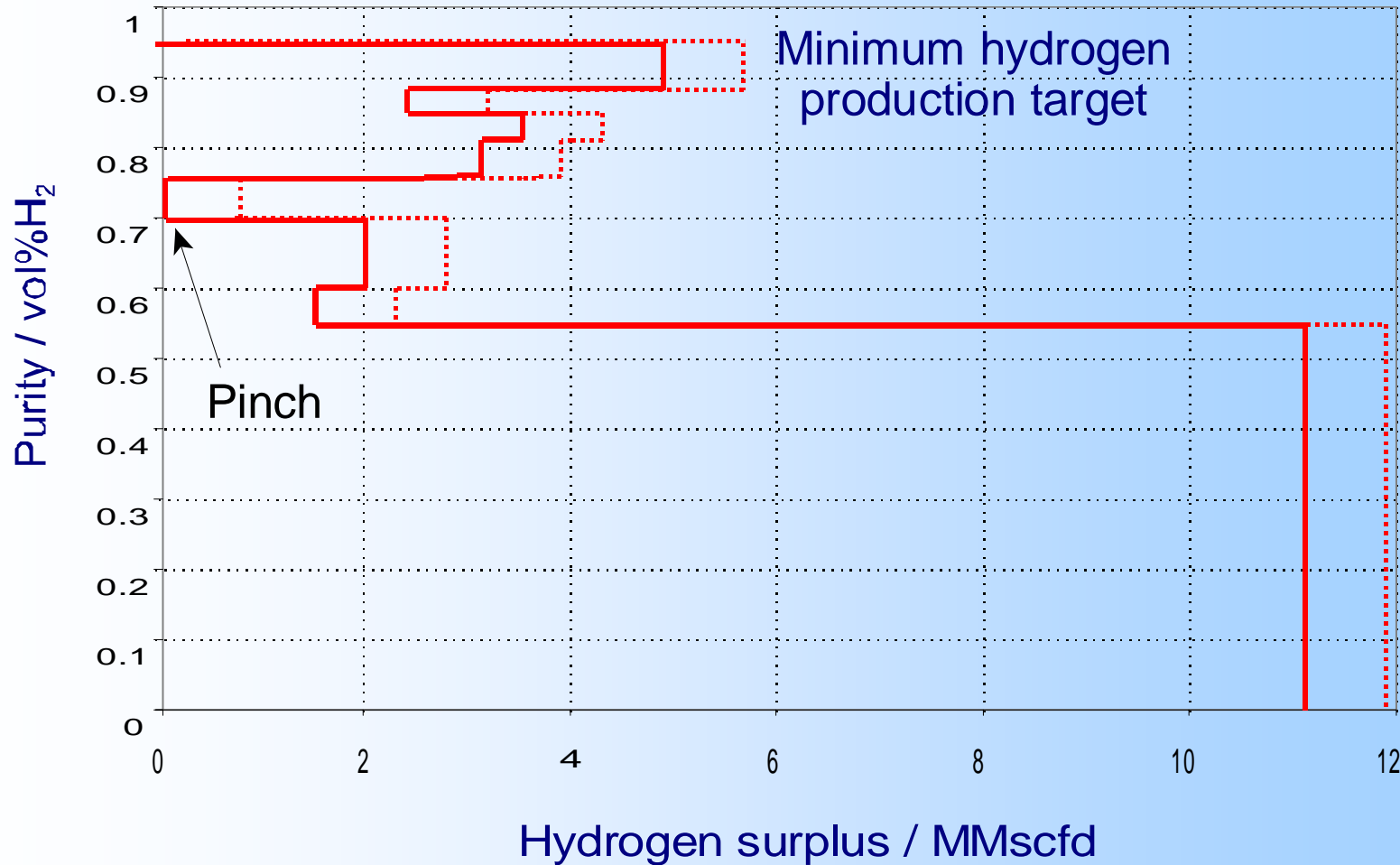
Hydrogen composite curves

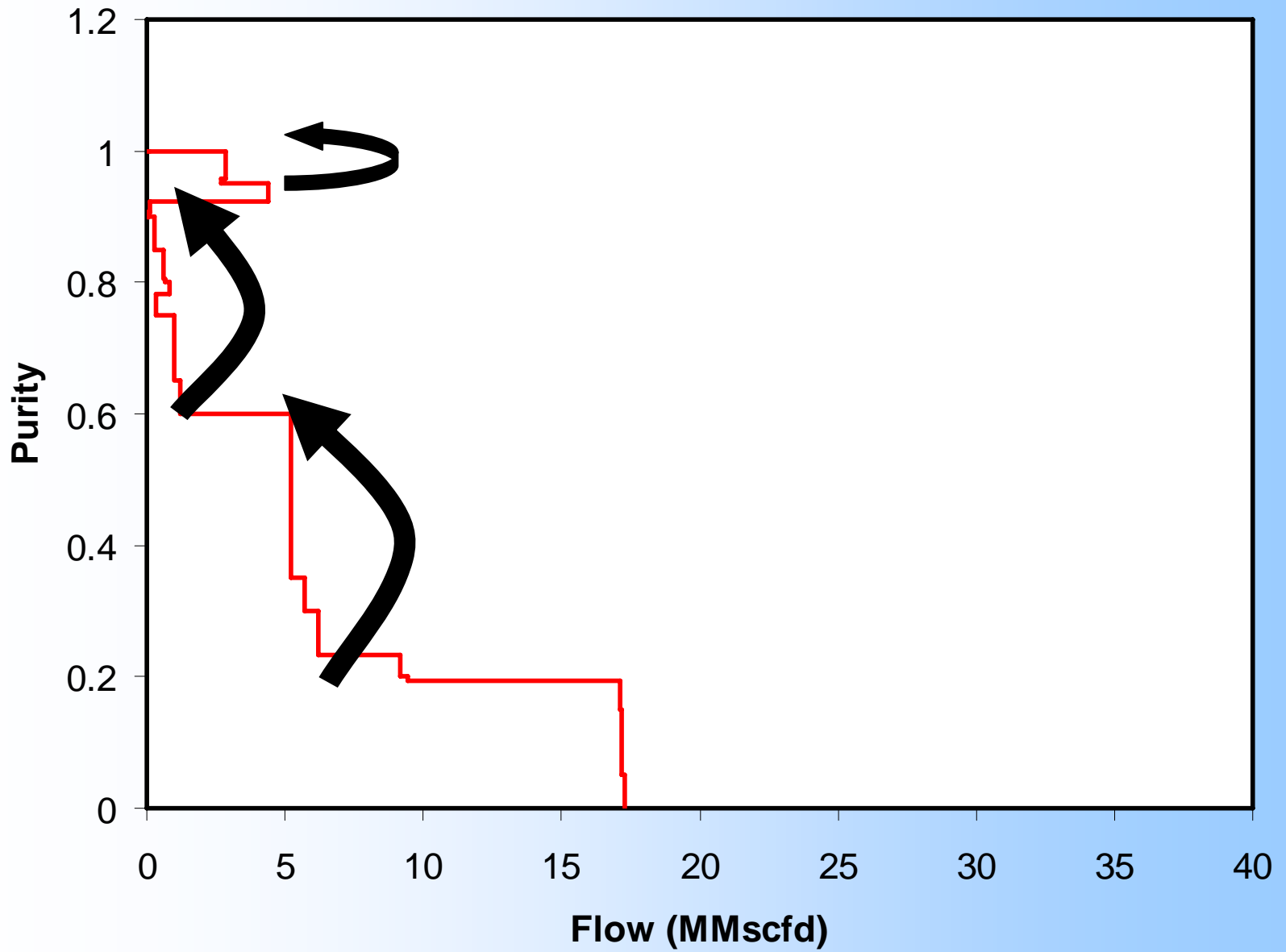


Hydrogen surplus diagram

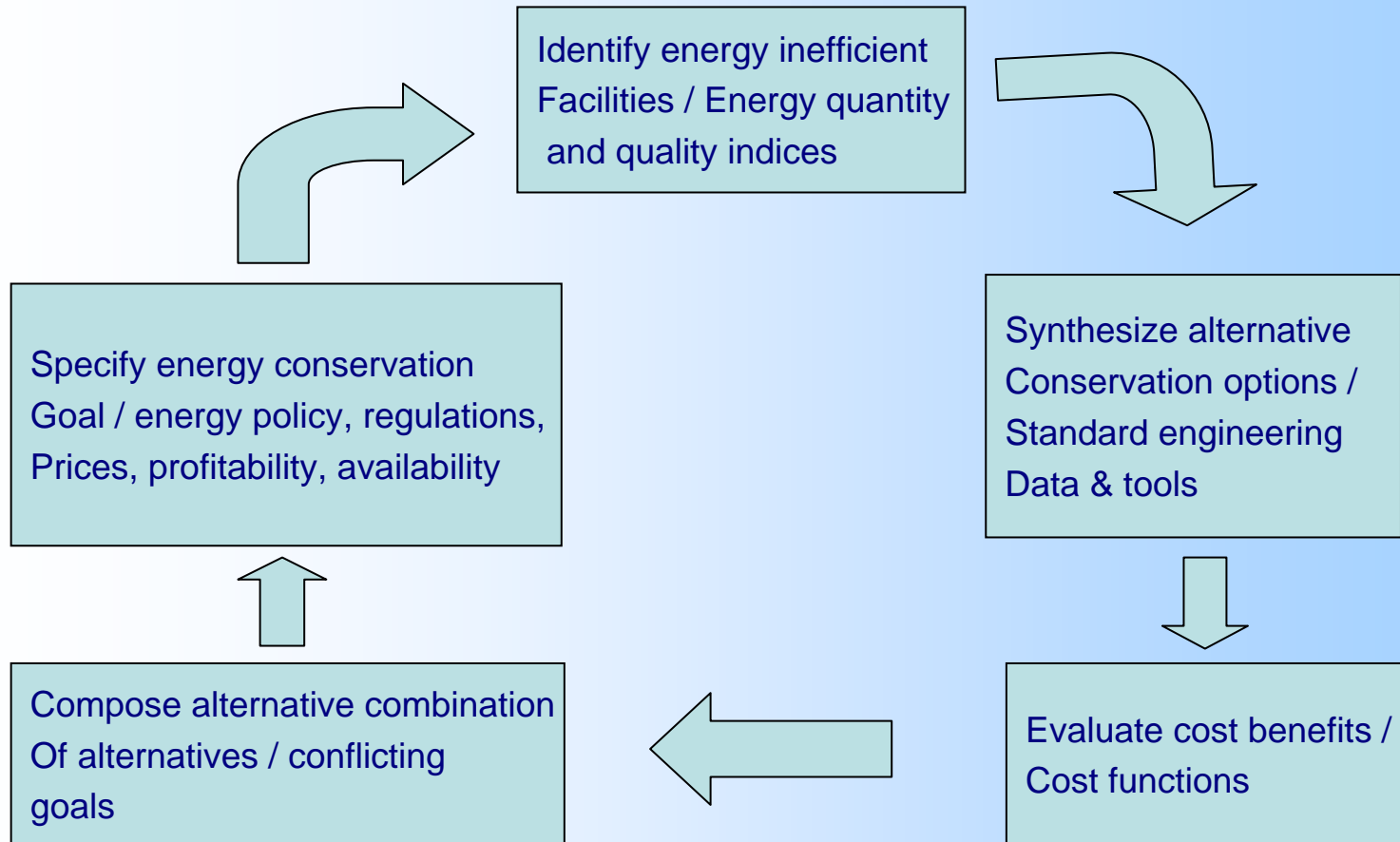


Hydrogen surplus diagram





Comprehensive energy management



ENCON tools at EIL



- In-house developed Excel based tools for:
 - Pump, compressor, fin fan coolers performance
 - VSD applications
 - Fired heater and boiler efficiency estimations
 - CHP model tailor made for specific site
- In-house developed Pinch analysis tools for:
 - HEN design and retrofit
 - Distillation column energy analysis
 - HEN monitoring and targeting
- UMIST suite of softwares for process integration

Conclusion



- Target both resource and energy conservation
- Adopt systems approach of analysis
- It is an ongoing dynamic process
- Update data base, cost functions regularly
- Evaluate every possible opportunity
- Finally.. ENCON is every one's business



Thank you

